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INSTRUCTOR/OPERATOR DISPLAY EVALUATION METHODS

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Final Report

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This technical report has been reviewed and is approved for publication.

WARTY B. ROSKWAY. Technical Director Operations Training Division

RONALD W. TLRRY, Colonel, USAI Commander

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The purpose of this study was to develop an objecti	ye, systematic technique for evaluating alternative formats for
The displays to be used at the instructor/operator star monitoring task was designed which exercises many of	tion (IOS) of a flight simulator. A benchmark performance the skills used by an instructor at a remote IOS. Measurement
techniques were developed for assessing performance of	the task. The techniques were demonstrated by using them to
compare two popular display formats: digital readou	ts versus repeater instruments. Three of six variables were [
monitored with greater accuracy and comprehensiven	ess using repeater instruments than digital readouts. For the [
other three variables, there was no difference between	display types. Significant effects were caused by both the type
of maneuver being flown and the type of question become	neing asked in administering the measurement method. We iderable merit as a method of evaluating display formats. In
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Jollow-on studic, additional investigations should be conducted on the specifies of the measurement technique and the possible effects of memory on results.

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In contemporary flight simulators, cathode ray tube (dkl) displays are typically used to display flight information to the instructor/operator. However, no one knows the best formats for displaying this data. Designs are usually based on an engine r's best guess in light of previous experience. As a result, displays are often difficult to use, and too much of the instructor's attention is consumed in merely searching for needed information. The Air Force has initiated a series of studies aimed at systematizing the design of the instructor/operator station (105) and improving the utility of associated displays. The purpose of this particular effort was to develop techniques for objectively evaluating alternative formats by assessing their impact on the instructor's performance.

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The approach was to develop a way to measure the instructor's performance on selected tasks. By this means, the effects of alternative display formats could be assessed by having subjects perform instructor tasks using the different displays and comparing the resulting performance measures.

The specific task selected was monitoring the pilot's performance,

i.e., observing and assimilating the current flight conditions and progress by watching the display. We developed a denomiark performance monitoring task that we could repeat in an experimental setting. To do this, we used several prerecorded flight segments to drive the display to be evaluated. The subject was required to carefully observe the display. At the conclusion of each segment, we asked specific questions of the subject to test the observations he was capable of making with that display. We reasoned that the success with which a subject is able to make consistently accurate observations is an indication of the display's value in supporting the performance monitoring task.

Specifics

We recorded several flights of each of five basic maneuvers: climb, descent, level turn, climbing turn, and descending turn. For each maneuver, we designed questions to assess the accuracy and comprehensiveness of the subjects' observations during the replay of the segment. These questions concerned maximum and minimum values of key variables and their values at strategic points in the maneuver. The questions were categorized into four types to distinguish whether they pertained to ranges or exact values of variables and whether they concerned observations over a span of time or at one specific time in the maneuver.

Subjects consisted of twenty C-lbD and C-l41 pilots from McChord Arb, Washington. They were not told what maneuver they were going to boserve. Instead, they were advised that they were to watch the display

and be prepared to answer questions about their observations regarding the values of major variables during the flight. Using a randomized design, we tested each subject using each of two alternative displays: digital readouts and repeat instruments. Flight segments were randomly selected and replayed on the display being tested. After each segment, the experimenter asked the test questions orally and recorded the responses.

Results of interest concern poth the utility of the overall method and the particular comparison of the two displays tested. We concluded that the method is extremely promising for evaluating displays. Our experience suggests some changes need to be made in the particular questions asked and the measurement method used. But the concept of the perconneck task approach has been clearly demonstrated as worthwhile.

Although the intent was to evaluate the methodology rather than achieve a meaningful comparison of displays, it is still of interest to see what the tests revealed. We found that questions regarding pitch, airspeed, and vertical velocity were answered more accurately with the repeater display than with the digital readout display. For questions on roll, heading and altitude, there was no significant difference between the two displays.

For pitch, both the type of maneuver and type of questions produced significant effects. Differences between the two displays occurred only in the climb and climbing turn. Maneuver type also produced a significant effect on airspeed questions. As might be expected, errors

were smallest for the level turn. For heaving, just the opposite was true, i.e., errors were greater for the level turn than for any other maneuver type.

The type of question produced significant effects for five of the six variables, airspeed being the only exception. On roll, for example, questions on the extremes of roll during the segment had the largest errors, and questions asking for a single value of roll at a specific point had the smallest errors. Other interesting results were found for the remaining variables, but there is no way to rationalize all the findings without additional study.

There was no strong correlation between elapsed time from event to question and the magnitude of errors. However, this is not a conclusive result because the study was not designed to treat elapsed time systematically. This should be studied further before extensive use is made of the method.

In conclusion, the penchmark task approach appears to be an excellent way to evaluate the comparative effectiveness of displays. Additional research needs to be performed on the question set, the particular measures used, and the possible effects of memory on task performance.

PRETACE

This seeds was conducted under Project (114, "Simulator Techniques for Nincrew Training," Task 6114-23, "Advanced Simulator Concents." Ms. Patricia Eroon was Project Scientist and Mr. Patrick Price was Task Coentist. Mr. Neel Schwartz was work unit and contract manager for the Nin Force.

The contractor conducted two distinct studies covering this work. The first study is documented in Appendix 0, and the second study constitutes the bulk of the pain text of the report. The two study reports were reported slightly by Ms. Knoon and Mr. Schwartz of Affall for preparation of this convergenceive report.

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Introduction

The Air Force needs an chiective technique for evaluating displays to be used at the instructor/operator station (IOS). The customary displays mode has been the use of repeator instruments, displays that, for the most part, duplicate those used in the cockpit. Alternative modes of information display may be more effective, but there must be some ways of establishing relative effectiveness before a decision to select one can be made intelligently. Some standard test is required for determining the relative effectiveness of display bethods.

The establishment of quidelines for designing and estating IOS displays cannot be accombished by reference to pertinent literature because the relevant data do not exist. This is often the situation when the specifications and recommendations arely to many faceted complex activities such as the work of the instructor milet (IP).

The goal of this study is to devise a nethod for determining IOS display effectiveness and for developing guidelines for display engineering in conformance with human skills and limitations. The approach is to select characteristic monitoring activities of the instructor/operator (IO) located at an IOS remote from the simulator and to develop a benchmark task based on these activities. This task was then performed by subjects using one of the alternative displays to be evaluated. Objective, quantitative performance measures on the task were computed and used to make inferences about the utility of the display in supporting the instructor's monitoring task. The technique was demonstrated by using the evaluate two display techniques: digital readouts versus repeater instruments.

II. Cack round

This is the second of two studies supported by AFPPE to develop a technique for the evaluation of displays to be used at an IOS associated with milet training in simulators. In the first study, the basic methods were developed and exercised in a prefiningry denonstration. This first study is documented in Appendix G of this report. The results of the first study showed that the concent of the benchmark task should be of meal value in the official assessment of IOS display effectiveness. The intent of the benchmark task is to provide the basis for a quantitative measure. tent of display effectiveness, while at the same time permitting the researcher to determine the limits of human abilities regarding merception and retention of visually displayed information. It should be directed most straightforwardly to the activities of the IP. On the other hand, meater congrality of the findings from the Lenchmark task requires that lasic human abilities be tapped for a wider application of the results to future IP operational tasks. It is a task whose essential characteristics concern short-term recall abilities, while being constructed in the framework of fright perfectioner conitering by an ID.

In the first study (see Annendix C), constions were generated to require a sincle answer, e.e., the maximum or minimum indication for some

selected flight parameter or the value shown at some identifiable noint during the flight segment. In the second study, the categories of questions were treated systematically, with each of four question types represented once for each maneuver type for each flight parameter (see Figure 1). The inclusion of flight indication ranges throughout the flight segment and over a limited portion of it (question types 1 and 2) was made to represent more realistically the monitoring requirements of the IP.

The first study used a "Multi-Mission Simulator" cocknit analog display with a cathode ray tube digitial display mounted above the instrument panel, where one or the other display was covered during the presentation of a flight segment. For the second study, a remotely piloted vehicle (RPV) control panel simulator was used. The arrangement of instruments and positions of the digital indicators on the CRT were the same in both studies but the RPV simulator was more convenient for the subject and experimenter because of the quality of lighting and wood table surface for writing and leaning on elbows during the segments. The RFV simulator also allowed the experimenter to be located closer to the subject, aiding communication.

The four subjects who served in the first study were drawn from the Crew Systems organization of Logistics Systems and Support in the Boeing Aerosapce Company and had quite heterogenous flying experiences. Included was a young person with only 40 hours of solo time in a light general aviation aircraft, as well as one subject whose flying time was mostly in helicopters and two other pilots who had flown a wide range of fixed wire aircraft, from early World War II equipment to multi-engine iets.

In the second study, the 20 milots serving as observers in the study were all currently flying either the C-130 or the C-141 aircraft. They had experience more directly relevant to fir Force interests than did the four subjects in the earlier study.

In the earlier study, each subject made 30 responses, 40 with each of the two displays. In the second study, each subject made 240 responses distributed evenly between the two display types; thus the experimental variables could be treated more systematically. For example, the earlier study was not designed to include questions about all six flight parameters after each flight segment was presented. In the second study, all six were included each time.

The most important area for improvement was in the kinds of data analyses that could be performed on the responses. It was apparent that the analysis of variance (ANOVA) was desirable for what could be shown about interactions among variables, as well as main effects. The larger, more systematic study permitted the demonstration of such interactions. Another benefit from the second study is the ability to do correlational analyses.

		TEMPORAL AS	SPECT
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UE ASPECT	RANGE	What were the extremes of airspeed in the flight segment? Type l	What was the change in airspeed in the transition to level- off? Type 2
NUMERICAL VALUE ASPECT	SPECIFIC	What was the highest airspeed during the flight segment? Type 3	What was the airspeed just prior to the trans- ition to level-off? Type 4

Figure 1. Sample categories of questions. (Maneuver: Altitude Change)

Much of the improvement in the second study data analyses was related to the treatment of the data in terms of absolute error instead of error tolerance limits. That is, the difference between the displayed altitude, for example, and the reported altitude (in feet) was the datum to be included in the analysis rather than a dichotomous scoring technique of right vs. wrong based on an arbitrary division point. Other flight parameters were treated similarly.

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Another goal in the second study was to develop a single measure of display effectiveness. This was to be based on a transformation of raw error scores into standard scores which assume a normal frequency distribution for each flight parameter. Standard scores are in standard deviation units, i.e., the deviation of the score from the mean value is divided by the standard deviation. Thus, a deviation equalling the standard deviation has a value of 1.0 regardless of the size of the mean or the standard deviation in the original units. The assumption of a normal distribution is accompanied by an assumption of equal importance of all measures to be included in a composite score taken as a figure of merit.

The variable of time interval between the occurrence of a flight indication and the end of the flight segment (when the questions were presented) was not analyzed in the earlier study but it was included in the study reported here.

In summary, a number of changes were made to improve the benchmark task evaluation: the test content, the testing environment, the subject population from which the larger sample of 20 subjects was drawn, the experimental design, the treatment of data as continuous rather than discrete, the use of analysis of variance and correlation techniques, and the collection of more complete data amenable to more sophisticated analyses. Of these, the most important were (a) enlarging the test and improving the questions, (b) gathering more data from a more qualified and homogeneous group, and (c) data analysis.

III. Research Methodology

The results of these studies are to be applied to the evaluation of IOS displays designed for the monitoring of pilot performance when the instructor and the student are not together, as would be the case with a single-place training simulator. Of the many activities a pilot may perform during a mission, e.g., weapon delivery, none is more basic than flight management. For this reason, an important part of the IP's task is to monitor the student pilot's flight performance.

The information chosen for display in this study was that shown in what is sometimes called the "basic T" of flight instruments. The horizon-tally aligned airspeed indicator, attitude indicator, and altimeter are the crossbar of the "T", while the heading indicator is centered below these three instruments. They are generally positioned in the instrument panel directly in front of the pilot so that they are easy to scan with little or no change in head position from that used for forward extra-cockpit viewing.

The display modes selected for the validation of the benchmark task were repeater instruments and a digital presentation on a CRT. The repeaters are analog displays that require scanning of a type different from that used for the digital reacout. A well experienced user of this kind of instrument frequently ignores the numbered dial when reading the pointer indications. An all-digital display cannot be scanned in the same way; it must be read by specifically noting the displayed numbers. These widely disparate modes of display were considered to be good candidates for the validation of the benchmark task.

Maritangue

In the present study of IOS display evaluation methods, the basic "T" configuration mentioned above and an added vertical velocity indicator (VVI) were used. The VVI is an important indicator of altitude change in that it permits the pilot to set the controls so that level flight or ascent/descent at a constant rate is accomplished by reference to a steady state condition rather than a uniform change in altitude indication. Furthermore, the VVI, like the altitude indicator example of the type of analog display in which the orientation of a pointer or a line (relative to a coordinate system based on the instrument panel) is usually of more interest than the actual numerical value of the indication. These flight parameters are displayed to the "experimental IP" (instructor pilot) for assessment of pilot performance as reflected in his recall of specific indications occurring during the flight segment.

The maneuvers represented on the display were of five different types. They encompass the group of maneuvers which comprise the tactics of combat and weapon delivery as well as general aircraft control. The basic maneuvers are climb, descent, level turn, climbing turn, and descending turn.

Flight segments were between 1 and 3 minutes duration. After the flight segment had been presented, the "instructor pilot" was asked to report on such indications as the maxima and minima of flight parameters or on indications occurring at specific places during the maneuver. In the preceding study, the subjects were asked a series of questions which were a random selection of those questions appropriate to the flight segment just presented. The current study included questions from all six flight parameters: airspeed, pitch angle, bank angle, altitude, vertical velocity, and compass heading. Thus all flight parameters were represented in the questions following the presentation of each flight segment to permit a greater amount of comparison between flight segments/ maneuvers. Appendix C contains all of the test questions along with correct responses and question type designators (as shown in Figure 1).

Each experimental subject (pilot) was presented four examples of five maneuvers and asked questions concerning the flight indications at various points and over various spans of time during these maneuvers. The questions required the subjects to remember extreme values of specified flight parameters or to recall a flight indication which occurred at some particular point in the flight segment. The four examples of each maneuver allowed the four types of questions to be presented an

equal number of times. Recordings of the maneuvers were made on magnetic tape. Each example of a maneuver was "flown" separately so that the subjects would not be seeing identical flight indications over the four examples of a given flight maneuver. This reduces effects of familiarization with the path flown and the corresponding flight indications. Where such learning effects occur, unwanted variability tends to obscure the experimental effects under study. Learning does occur in any experiment where there are repeated trials. The subject learns something of the approach to measurement used by the individual or group who designed the experiment and of the nature of the task to be performed. In the present study, each flight segment was presented twice to each subject, once with traditional analog instruments (called "round dials" by the pilots) and once on the CRT in digital format. While this repetition of each flight segment may have facilitated recall of the contents of the display, the randomization of flight-segment-by-display-conditions would have minimized any systematic effect of this repetition on recall, i.e., while the variance may have been affected by duplicating a flight segment for the alternate display, this effect would not result in a bias in favor of one or another major variable other than that arising from chance.

The design of any study is generated within the context of limitations of time and other resources. In the present instance, the major concern focused on the feasibility of the approach, namely the development of a benchmark task which could serve as a standard for the evaluation of IOS displays. Maximizing the potential information derivable from such a study means balancing the effects that are to be observed against the potential diminution for the demonstration of the effects of higher priority variables. For example, the subjects were asked to monitor only a few of the types of information that an instructor pilot might have at the IOS. The display modes (analog and digital) and the manner in which the information was presented were somewhat arbitrarily chosen. The analog and digital displays used in this study were not themselves the objects of study; the object of study was the IOS display evaluation technique.

The experimental variables are represented in the accompanying block diagram, Figure 2.

IV. Experimental Design

The design of the present study differs from the previous one primarily in that it utilized a larger number of subjects (20 current Air Force pilots as opposed to four non-military pilots) and yielded three times as much data per subject. The design permits a look at the interactions among the several variables. Of particular interest is the time factor, that is, the time during the flight segment to which the question applies and thus the length of time during which the information must be retained.

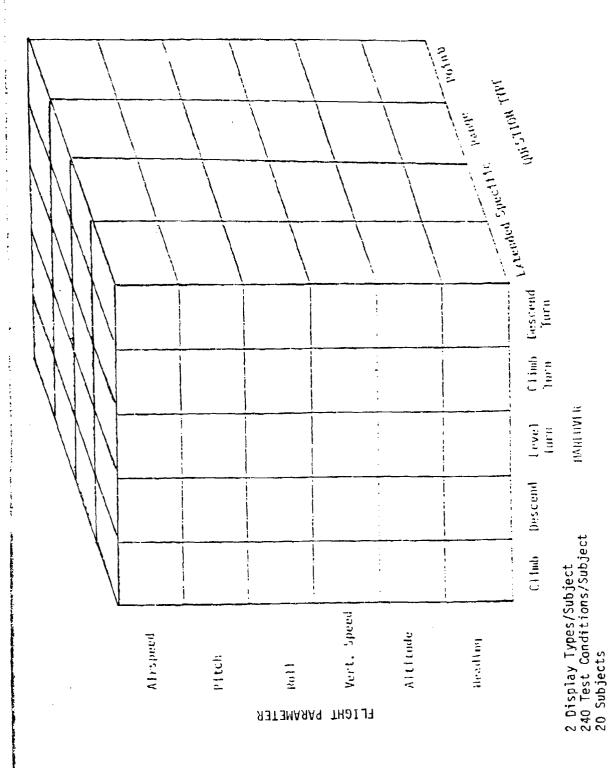


Figure 2. Experimental variables.

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The time factor would be expected to interact with display format and type of question. Range-type questions might prove easier to answer. The six questions were generated by reference to strip chart recordings of the six flight parameters displayed for each flight segment. These questions and the correct answers are shown in Appendix D. Question types were counterbalanced to insure their equal representation across maneuver types and flight parameters for each of the two displays. Questions were devised on the basis of subjective decisions regarding the probable clarity with which they would be interpreted by the observer pilots.

In some cases, the questions referred to relatively minor variations of flight indication because of the path flown by the simulator pilot. For example, if the maneuver was a straight climb, successful pilotage would result in a constant heading, though the design of the study would require the generation of a question regarding change of heading.

The time factor was also taken from the strip chart of the various flight parameters. The elapsed time between the occurrence of a requested indication and the end of the flight was noted. Though this datum did not accurately indicate the time between the flight indication and the question pertaining to it (because of sequencing of questions in the post-flight-segment inquiry period), nevertheless it was chosen as the most reasonable approximation, given the alternative of a cumbersome measurement procedure.

The order in which the various flight parameter questions were asked was randomized independently for every flight segment and for each observer pilot. The type of question associated with a given maneuver was counterbalanced across the four examples of that maneuver but remained the same for all observer pilots. The forty flight segments were randomized independently for each observer pilot. Display type and maneuver/replication were thus randomly variable according to a computer-generated random order (2 displays by 5 maneuvers by 4 question types). These are contained in Appendix E.

The primary statistical analysis used for the determination of the adequacy of the IOS display evaluation technique for discriminating between display types was the analysis of variance. This type of analysis was chosen because it permitted the main effects and the interactions among them to be seen. Additional analyses included correlations between display types for each flight parameter and item-test correlations of the mean error for each question with the mean of the total errors for each flight parameter. Error magnitude correlation with time interval was also calculated.

V. Procedure

Those who served as observers in this study were Military Airlift Command pilots from McChord AFB south of Seattle, Washington. Eighteen were C-130 pilots and two were C-141 pilots. All were cooperative and

seemed interested in the problem of IOS displays, with the reservation that they tended, in an understandable way, to react to the task within the frame of reference of the MAC pilot rather than as an instructor at an IOS associated with a single seat, high-performance fighter simulator. Because of a belief that the nature of the task required of them would be performed best if they had an opportunity to get away from it periodically, two pilots served alternatively in one-hour sessions. (It soon became evident that this was a prudent step as the pilots wearied at the task after about an hour). Thus, one pilot would observe the displays and answer questions while the other could view nearby simulation facilities, have a cup of coffee in the cafeteria, or read some material of general interest in the laboratory area.

The 40 flight segments comprising the complete session were divided into four sub-sessions of 10 each. These sub-sessions were a little less than an hour's duration and two subjects could be run in a single day, each serving 4 ho rs at the experimental monitoring task. The McChord AFB pilots were assigned to the 1 day temporary duty to serve in the study on the basis of availability. The average age of the pilots was 29.6 years with a standard deviation (S.D.) of 3.0 years. Total flight hours averaged 2248 (S.D. = 858). Current equipment for 16 pilots was the C-130 in which they averaged 1128 hours (S.D. = 135). All had flown the T-37, ranging from 80 to 1700 hours and all listed time for the T-38. Ten of the 20 pilots also listed civilian light aircraft time.

After arriving pilots had gone through the required check-in procedures, the experimenters led them to the nearby laboratory facility where the display equipment for the test was located (Visual Flight Simulation Laboratory). Each pilot was asked to fill out a brief form (Appendix F) for information about his age, current equipment, and flying time in all types of aircraft. The observer pilot was then given a copy of instructions for performing the task (Appendix A). This briefing material included a general explanation of the goals of the study and a statement to the effect that the pilots were not being evaluated regarding their personal skills but that the display evaluation technique itself was the subject of the investigation.

After reading the instructions, the pilot was asked whether there were any questions about them. The next part of the task familiarization included showing the pilot both of the display types: i.e., analog instruments and digital presentation of the CRT. The pilot was then shown how to cover either of the displays for the viewing of its alternate. It was here explained that the display mode used for any given flight segment was determined by randomization. This was also true for maneuver type, question type, and flight parameter. The presentation orders for each pilot are shown in Appendix E. Flight segment numbers were assigned such that designators 1 through 20 referred to the analog instrument display mode and designators 21 through 40 to the CRT digital display mode. The method of ordering the presentations of the flight segments is called random without replacement, i.e., no flight segment (as designated above) occurred twice for a given observer pilot on the same display.

Prior to the initiation of the first flight segment, the experimenter pointed out the flight instruments to be used and compared them with the same indications as shown on the CRT in the digital display mode. Figure 3 shows both display modes. Figures 4 and 5 show each display separately. The experimenter pointed out the locations of the pitch and bank angle indications on the CRT because the digital attitude display is not integrated as it is in the analog instruments.

The CRT was positioned above the instrument panel with the bottom of the scope at eye level. The pilot's eyes were located about 53 cm from the screen or instruments. Obviously, there were variations in the eye position because of body dimension differences among pilots or different postures.

The tube face was 30 cm wide and 22.5 cm high, while the displayed information was 20 cm wide and 7.5 cm high. Approximate center-to-center distances between adjacent flight indications were between 5 and 6 centimeters. Symbol size was adequate for easy reading.

The analog instruments extended horizontally 38 cm, vertically 22 cm. The ADI was the largest instrument at 10.7 cm width, while the heading indicator just below it was second largest at 9.3 cm width. The other three instruments, i.e., airspeed indicator, vertical velocity indicator, and altimeter, were all 7.3 cm wide. Center-to-center distances from the ADI to the other instruments were 15 cm to the altimeter, and 13 cm to the heading indicator.

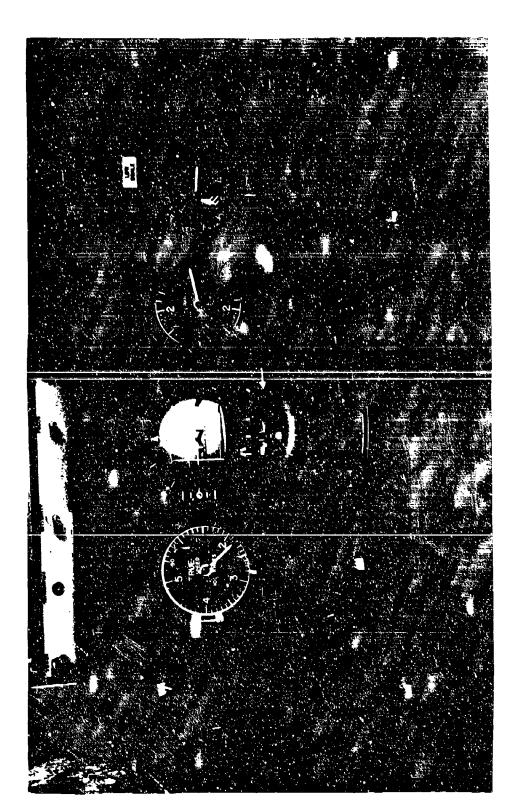
A mask for the CRT was made of Fome-Cor and had a hinged door which could swing to one side to expose the face of the CRT. When the CRT was being used, a mask was set in place to occlude the analog instruments. This method permitted the use of simpler equipment design than would have been necessary if one mode had to be disabled while the other was being used.

Before observing the final 10 flight segments, each pilot was asked informally to comment on the conditions of the test. Their comments were recorded on tape (with their awareness) for later study. They were asked to compare the two display modes for each of the six flight parameters and to add anything they might have to say about the quality of the questions they were asked, the reasonableness of the simulation, the quality of the test environment, or the conduct of the test.

Although the subjects were encouraged by the experimenter to keep trying if they expressed doubts about their performance, they were told nothing about the correctness of their answers. If anyone seemed hesitant about answering a question, the experimenter asked that pilot to offer a quess.



Figure 3. Photograph showing both displays.



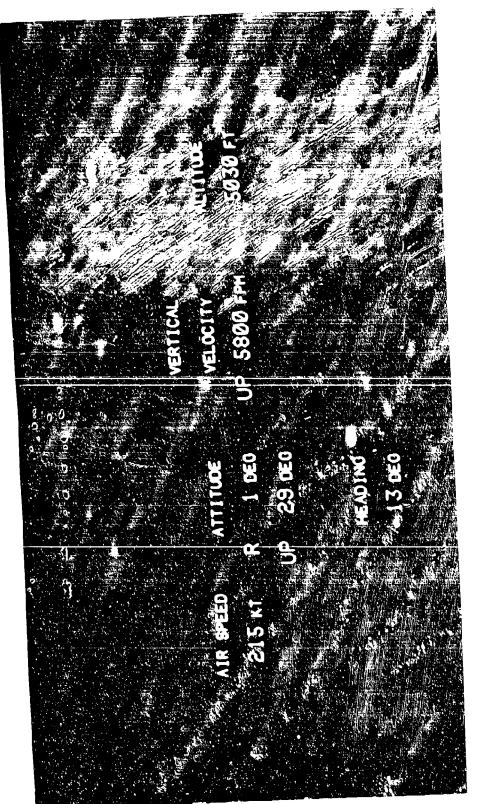


Figure 5. Photograph showing digital display.

VI. Results and Discussion

The independent variable of greatest interest was display mode, analog instruments vs. CRT digital format. To see the effect of this variable on the monitoring task, a separate ANOVA was computed for each of the six flight parameters. The dependent variable in each analysis was the size of the errors in the responses to the questions, the absolute error magnitude. Appendix B contains the raw data, that is, the responses actually given. The score was the absolute difference between the response shown in Appendix B and the correct response for that question shown in Appendix C.

To equate the four question types, the double-answer questions were treated as two separate questions and the sum of the errors for the two were averaged to yield a single score comparable to the single answer questions. These data were used, along with the errors from single-answer questions, in the ANOVA for the six parameters.

The ANOVA and means of pitch angle recall errors is shown in Table 1. Pitch angle responses were given with smaller error when the observer had been viewing the flight segment on the analog instruments compared to his responses after a digital format presentation on the CRT (p < .05). While the difference in error is small, 3.04 degrees for analog and 3.64 degrees for digital, the size of the error difference is not as important as the demonstration that a short-term memory task like this one can differentiate between display types.

The type of maneuver is also a significant main effect (p < .05). This is expected because of the correlation between maneuver type and variation in flight parameter values. Question type was also significant (p < .05) for the pitch angle ANOVA, with the type asking for the extremes of pitch throughout the flight segment (Type 1) yielding smaller error magnitudes than the other three types. The reason for this is not clear, especially in light of the fact that the third type of question asking for just one extreme (half of the Type 1 question) yielded the largest error of the four.

The display type by maneuver interaction is significant (p < .05) for the pitch parameter and the means suggest that the difference in favor of the analog display format occurred primarily with the straight climb and, to a lesser degree, with the climbing turn. The superiority of the analog display for pitch information is thus not uniformly evident for all five maneuvers, not appearing in the cases of level turn, descent, and descending turn. Maneuver by question type is also significant (p < .05). For example, type 2 questions yielded the worst performance of all 20 combinations (four question types x five maneuvers) with the straight climb maneuver but the best of all with the level turn maneuver.

Finally, the significant (p < .05) display by maneuver question type interaction means that the maneuver by question type interaction is different for the two displays, being more marked for the distal than for the analog display.

Table 1

ANOVA and Means of Pitch Angle Recall Errors for Display
Type (D), Maneuver Type (M), Question Type (Q), and Interactions

.340 (-)/		, , , ,	• • • • •	•	
Source	Error Term.	Deg. of Freedom	Sum of Squares	Mean Squares	Ratio
Subject Display Ty Maneuver Question T SD	SM	19 1 4 3 19	154.363 73.811 962.919 235.264 134.213	8.12¢ 73.811 240.730 78.755 7.064	10.449* 37.47&* 10.757*
SM DM SQ	SDM	76 4 57	488.164 217.494 417.303	6.423 54.373 7.321	11.541*
DQ MQ SDM SDQ	SDQ SMQ	3 12 76 57	23.594 1811.072 358.059 359.863	7.865 150.923 4.711 6.313	1.246 19.484*
SMQ DMQ SDMQ	SDMQ	228 12 228	1766.036 135.224 1148.630	7.746 11.269 5.038	2.237
*p < .05	Climb (1)	Climbing Turn (2)	Level Turn (3)	Descent	Descending 1:rn (i)
	5.425	3.188	3.144	2.712	2.238
		DISP	LAY BY MANEL	IVER	
Analog Digital	4.100 6.750	2.938 3.438	3.175 3.112	2.700 2.725	2.275 2.200
		QUESTION	TYPE BY MAN	IEUVEK	
(1) (2) (3) (4)	4.825 7.825 6.725 2.325	1.925 4.300 3.250 3.275	1.950 1.400 1.775 7.450	1.750 3.175 4.175 1.750	1.700 1.550 3.250 2.450
	DI	SPLAY BY QUE	STION TYPE E	BY MANEUVED	
Analog-1 2- 3 4	3.300 5.200 5.900 2.000	1.800 4.200 3.000 2.750	1.350 1.750 2.000 7.600	1.750 3.050 4.300 1.700	2.150 1.250 3.309 2.400
Digital-1 2 3 4	6.350 10.450 7.550 2.650	2.050 4.400 3.500 3.800	2.550 1.050 1.550 7.300	1.750 3.300 4.050 1.800	1.250 1.850 3.200 2.500
PALASIC		<u>Analog</u> 3.038		<u>igital</u> .645	
QUESTION .	TYPE: (1) 2	.430, (2) 3	.650, (3) 3,8	335, (4) 3.450)

Table 2 shows the ANOVA and means of roll angle recall errors. Roll angle recall performance was not significantly different for the two displays. Maneuver types showed differences since those involving no turns varied little from zero roll. Question type showed significant differences (p < .05), with Type 1 (extremes of roll during the flight segment) associated with the largest error and Type 4 (single indication at a specified point in the flight segment) the smallest error. As both maneuver and question type were statistically significant, so also was the interaction between these two factors (p < .05); the pattern of this interaction is difficult to interpret, however. One might speculate that in piloting an aircraft with the standard artificial horizon, there is little concern about the specific number of degrees of roll, and that the question asking for this number would tend to place that kind of attitude display at a disadvantage. Nevertheless, there was no significant difference in favor of the digital format.

Table 3 shows the ANOVA and means of heading recall errors. Heading recall was not significantly different for the two display formats. Type of maneuver was a significant factor (p < .05) with the level turn resulting in far larger errors than was the case with other maneuvers. It should be pointed out that there was greater opportunity for error in heading recall with this maneuver because the heading change was about 180 degrees, as opposed to the climbing and descending turns which involved heading changes of 90 degrees. Question type significantly a fected heading recall performance (p < .05), with Type 2 (change in indication during some limited portion of the flight segment) resulting in the largest error. Type 3 questions yielded errors averaging threefourths the size of Type 2 errors, but the remaining two question types were associated with errors only two-fifths the size of Type 2 errors. There is a significant interaction (p < .05) between maneuver type and question type but the range of differences in the 20 combinations of maneuver and question type suggests the possibility of a serious artifact. The largest average error in the matrix was 132.25 for a Type 3 question on a level turn while the same type of question about a straight descent resulted in the smallest average error of 0.125. The heading recall data need closer scrutiny before they can be interpreted unambiguously.

Table 4 shows the ANOVA and means of airspeed recall errors. Airspeed recall performance was significantly better for the analog display format (p < .05). Maneuver type was again a significant main effect (p < .05) but the reasons for the differences observable in the data are not immediately clear. The average airspeed error for the level turn is about one-half that observed for three of the other four maneuvers and only two thirds of that for the remaining one. Though question type is not significant as a main effect, it does interact significantly with maneuver type (p < .05). The basis for this interaction is not apparent.

Table 5 shows the ANOVA and means of altitude recall error. Altitude recall errors were not significantly different for the two display formats. Maneuver type was significant (p < .05) with the level turn,

Table 2.

ANOVA and Means of Roll Angle Recall Errors for Display
Type (D), Maneuver Type (M), Question Type (Q), and Interactions

Source	Error Term.	Deg. of Freedom	Sum of Square	Mean Squares	F <u>Ratio</u>
Subject Display Type Maneuver Question Type SD SM DM	SD SM SQ SDM	19 1 4 3 19 76 4	1315.544 7.220 5294.918 746.885 1451.626 4561.660 128.523	69.239 7.220 1323.729 248.962 76.401 60.022 32.131	0.094 22.054* 4.528*
SQ DQ MQ SDM	SDQ SMQ	57 3 12 76	3133.751 307.470 2601.275 4725.688	54.978 102.490 216.773 62.180	1.891 4.700*
SDQ SMQ DMQ SDMQ	SDMQ	57 228 12 228	3088.623 10516.60 607.268 10463.18	54.186 46.125 50.606 45.891	1.103

^{*}p < .05

	Climb (1)	Climbing Turn (2)	Level Turn (3)	Descent (4)	Descending Turn (5)
	1.688	5.450	5.700	1.475	8.200
		QUEST	ON TYPE BY	MANEUVER	
(1) (2) (3) (4)	1.750 1.350 3.650 0.0	8.725 5.225 3.200 4.650	7.350 7.750 4.350 3.350	4.900 0.0 0.150 0.850	5.500 8.925 12.375 6.000

QUESTION TYPE: (1) 5.645, (2) 4.650, (3) 4.745, (4) 2.970

Table 3:

ANOVA and Means of Heading Recall Errors for Display
Type (D), Maneuver Type (M), Question Type (Q), and Interactions

Source	Error Term.	Deg. of Freedom	Sum of Squares	Mean Squares	F <u>Ratio</u>
Subject		19	94792.00	4989.051	
Display Type	SD	1	8026.441	8026.441	3.612
Maneuver	SM	4	125262.5	31315.63	8.198*
Question Type	SQ	3	84538.44	28179.48	5.066*
SD	•	19	42227.18	2222.483	
SM		76	290318.5	3819.980	
DM	SDM	4	7440.688	1860.172	0.541
SQ		57	317027.3	5561.879	
ρĝ	SDQ	3	2140.688	713.562	0.190
MQ	SMQ	12	536719.8	44726.65	10.178*
SĎM	,	76	261191.4	3436.729	
SDQ		57	214566.9	3764.332	
SMQ		228	1001952.	4394.523	
DMQ	SDMQ	12	26969.56	2247.463	0.804
SDMQ	-	228	637550.3	2796.273	_

^{*}p < .05

	Climb (1)		Climbin Turn (2)	ng Level Turn (3)	Descent	Descending Turn (5)
	23.631		28.256	50.875	15.256	19.069
			QUES	STION TYPE BY	MANEUVER	
(1) (2) (3) (4)	0.300 69.875 1.800 22.550		52 550 53.250 2.550 4.675	7.675 44.275 132.250 19.300	14.425 25.700 0.125 20.775	14.050 19.400 19.825 23.000
QUESTION	TYPE:	(1)	17.800,	(2) 42.500,	(3) 31.310, (4) 18.060

Table 4:

ANOVA and Means of Airspeed Recall Errors for Display
Type (D), Maneuver Type (M), Question Type (Q), and Interactions

Source	Error Term.	Deg. of Freedom	Sum of Squares	Mean Squares	F <u>Ratio</u>
Subject	60	19	7955.516	418.711	
Display Type	SD SM	1 4	1180.980 8909.305	1180.980 2227.326	4.415* 7.669*
Maneuver Question Type	SQ	3	1410.525	470.175	2,232
SD	34	19	5082.129	267.480	£, £J£
SM		76	22074.07	290.448	
MO	SDM	4	434.387	108.597	0.787
SQ		57	12004.95	210.613	
QΦ	SDQ	3	822.610	274.203	2.081
MQ	SMQ	12	7078.277	589.856	2.667*
SDM		76	10489.30	138.017	
SDQ		57	7511.195	131.775	
SMQ		228	50426.39	221.168	
DMQ	SDMQ	12	1205.227	100.436	0.615
SDMQ	,	228	37208.82	163.197	

p < .05

	Climb (1)	Climbing Turn (2)	Level Turn (3)	Descent (4)	Descending Turn (5)
	14.625	16.881	7.169	11.175	13.962
		QUESTIC	N TYPE BY	MANEUVER	
(1) (2) (3) (4)	9.200 13.300 16.750 19.250	16.600 14.425 19.750 16.750	9.225 4.725 9.350 5.375	9.600 15.150 12.925 7.025	10.825 21.825 12.375 10.825
DISPLAY		<u>Analog</u> 11.548		<u>Digital</u> 13.978	

Table 5:

ANOVA and Means of Altitude Recall Errors for Display
Type (D), Maneuver Type (M), Question Type (Q), and Interactions

Source	Error Term	Deg. of Freedom	Sum of Squares	Mean Squares	F <u>Ratio</u>
Subject Display Type Maneuver Question Type SD SM DM SQ DQ MQ SDM SDM SDQ SMO	SD SM SQ SDM SDQ SMQ	19 1 4 3 19 76 4 57 3 12 76 67	.45323E 08 .34915E 06 .17753E 08 .15627E 08 .66584E 08 .11866E 09 .59676E 07 .87436E 08 .16659E 07 .63764E 08 .14380E 09 .84865E 08	2385465 349155 4438392 5209320 3504444 1561343 1491920 1533975 555303 5313693 1892141 1488863	0.100 2.843* 3.396* 0.788 0.373 3.523*
DMQ SDMQ	SDMQ	228 12 228	.34393E 09 .22421E 08 .34215E 09	1508472 1868460 1500682	`1.245

^{*}p< .05

	Climb (1)	Climbing Turn (2)	Level Turn (3)	Descent (4)	Descending Turn (5)
	525.250	597.475	165.319	416.962	358.525
			N TYPE BY MAN	IEUVER	
(1) (2) (3) (4)	293.375 557.625 692.000 558.000	216.275 1751.625 129.375 292.625	202.625 214.250 100.900 143.500	211.575 472.375 430.400 553.500	369.500 202.800 477.550 384.250
QUESTION	TYPE: (1)	258.670, (2)	639.735, (3)	366.045,	(4) 386.375

as expected, associated with the smallest error. Question type was a significant main effect (p < .05) with Type 2 questions yielding errors averaging two-thirds larger than the next poorest question, Type 4. Maneuver interacts significantly with question type (p < .05) but a look at the matrix suggests cautious interpretation. On several occasions, the pilot not accustomed to reading a three-needle altimeter made errors as large as 10,000 feet.

Table 6 shows the ANOVA and means of vertical velocity recall errors. Vertical velocity indications were recailed significantly more accurately (p < .05) with the analog instrument than with the digital presentation on the CRT. The type of maneuver was again significant (p < .05) but not in any simple way, since the poorest performance occurred with level turns while the best occurred with straight climbs. Question type is a significant factor with this flight parameter, with the Type 3 question (single extreme value during the entire flight segment) showing two and a half times the error obtained with Type 2 (change during some limited portion of the flight segment). Display format interacts significantly with maneuver (p < .05), the largest difference between displays appearing with descending turns where the error with the digital mode was twice that with the analog instruments. Question type also interacts significantly with maneuver (p < .05) but not in any clearly systematic way.

The ability to recall information should be related to the elapsed time between the presentation of this information and the recall attempt. Table 7 contains the correlation coefficients for the two displays. In one analysis, error magnitude is compared with the time between the occurrence of the event in question and the end of the flight segment, and in the other analysis, this time period is converted to a percentage of the total flight segment. The coefficients which are significantly different from zero are identified by asterisks (p < .05).

Although 36 of the 120 correlations in the table as a whole are statistically significant, the largest is r=.526 which corresponds to an index of forecasting efficiency of 15%, % Efficiency = $(1-1-r^2)100$. This index shows the percentage reduction in errors in predicting performance from knowledge of the time interval between the event and the end of the flight segment, compared to predicting the mean performance for each time interval. Those correlations around r=.200 yield an index of forecasting efficiency of only 2%. It is apparent that there is no strong correlation between time interval and error magnitude.

The analog display mode shows significant correlations in seven cases when time interval is used for the analysis and in eight cases when this time interval is converted to percent of total segment time. Not unexpectedly most of these cases (six out of eight) overlap in the two methods of analysis.

The digital display mode shows significant correlations in 11 cases when the analysis is of time interval and performance and in 10 cases when percent segment time is used, all 10 overlapping with those showing significance in the time interval analysis.

Table 6:

ANOVA and Means of Vertical Velocity Recall Errors for Display Type (D), Maneuver Type (M), Question Type (Q) and Interactions

<u>Source</u>	Error <u>Term.</u>	Deg. of Freedom	Sum of Square	Mean Squares	F <u>Ratio</u>
Subject Display Type Maneuver Question Type SD SM DM SQ DQ MQ SDM SDM SDQ SMQ SMQ SMQ	SD SM SQ SDM SDQ SMQ	19 1 4 3 19 76 4 57 3 12 76 57 228	.4417906E 08 .1709749E 08 .2613584E 08 .1199948E 09 .2486242E 08 .1775190E 09 .1532442E 08 .1190743E 09 .1354378E 08 .2548061E 09 .1657711E 09 .165726E 09	2325213 17097490 6533960 39998260 1308548 2335776 3831104 2089022 4514592 21233840 1391724 1869694 1728193	13.066* 2.797* 19.147* 2.753* 2.415 12.287*
DMQ SDMQ	SDMQ	12 228	.3133226E 08 .3441272E 09	2611021 1509329	1.730

^{*}p < .05

	Climb (1)	Climbing Turn (2)	Level Turn (3)	Descent (4)	Descending Turn (5)
	725.844	1119.531	1274.081	1104.806	1077.519
		DISPLAY BY	MANEUVER		
Analog Digital	767.375 684.312	1004.375 1234.688	1108.712 1439.450	998.987 1210.625	691.375 1463.662
	QL	JESTION TYPE	BY MANEUVER		
(1) (2) (3) (4)	446.375 387.500 1757.000 312.500	1165.625 1307.500 516.250 1488.750	648.875 401.200 3350.000 696.250	616.875 482.850 1658.375 1661.125	963.875 768.700 996.250 1581.250
DISPLAY		Analog 914.165		<u>Digital</u> 1206.54	7

QUESTION TYPE: (1) 768.325, (2) 669.550, (3) 1655.575, (4) 1147.975

Table 7:

DISPLAY 1 - (Analog)

Correlations of Error With Segment Time Remaining

Maneuver/	Pitch	<u>Ro11</u>	<u>Heading</u>	Airspeed	Altitude	VVI
Climb	.306*	526*	041	.035	.106	.163
Climbing Turn	.138	223*	373*	.066	032	.131
Leve! Turn	249*	082	071	032	116	.153
Descent	367*	.176	.114	133	081	.139
Descending Turn	221*	.002	.072	365	117	130
Correlations	of Error I	with Perce	nt Segmen	t Time Rem	aining	
Climb	.278*	475*	.073	.027	.090	.122
Climbing Turn	.117	201*	358*	.061	043	.133
Level Turn	390*	010	009	009	126	.212*
Descent	252*	.227*	.112	129	080	.132
Descending Turn	104	.017	.061	336	104	088

DISPLAY 2 - (Digital)

Correlations of Error With Segment Time Remaining

Climb Climbing Turn	.485* .003	238* 188*	043 392*	.083 .234*	066 .019	.006 200*
Level Turn	287*	172	105	.003	081	.198*
Descent	107	,226*	048	193*	.006	.169
Descending Turn	179	155	088	237*	025	.018
Correlations	of Error N	Nith Perce	nt Segmen	it Time Re	emaining	
Climb	.517*	174	.044	.081	063	.070
Climbing Turn	023	~.199*	381*	.240*	.002	199*
Level Turn	268*	125	040	.027	039	.287*
Descent	. 174	. 284*	~.046	186*	.022	. 158
Descending Turn	168	140	121	240*	054	.005

p < .05

For the analog display, correlations of error with intervening time were significant in seven instances, only one of which is positive in sign. This instance occurred for the flight parameter of pitch in the climb maneuver. However, each correlation is based on six responses to four questions (see discussion of question types, section) by 20 pilots. While the magnitude of error in a response can vary widely among the 20 pilots, the corresponding time interval is fixed at a single value.

The content of a question was dictated mostly by the availability of an event involving the given flight parameter, that is, an event about which a question could be formed. The starting point for the generation of questions (Appendix C) was the detailed inspection of the strip chart records (Appendix D). The choice of question was further restricted by the question type it had to represent. The point in the time segment where occurred the event corresponding to the desired question left little or no choice for a balanced selection of time intervals.

The digital display yields results similar to the analog display in that the most significant correlations of error performance with time interval are negative (seven out of 11). Since the test is the same as that used with the analog display, the discussion of the results for the analog mode applies here as well.

If the results of the correlational analysis are accepted as meaningful on the basis of statistical probability even though the coefficients are not high, then it is assumed that there is a tendency for the subjects to remember earlier flight indications better than later ones. However the possibility that these results are due to artifacts in the flight segments as flown or in the test questions cannot be excluded.

The study was not designed to treat the elapsed time question in a systematic way. The lack of a strong correlation between error magnitude and elapsed time is therefore not a conclusive finding.

Item-Test Correlations

The item-test correlations are shown in Table 8. The error scores for question types 1 and 2 were the average of the errors in the two answers given. These were added to the error scores from question types 3 and 4 and total errors were summed across the 20 questions (five maneuvers x four question types) for the subject to obtain a single score on that flight parameter. The correlation coefficients range from .810 to .015 in magnitude, and 20 coefficients are negative. The lower the correlation, the less the question contributes to the total score and if the sign is negative, larger errors in responses to that question are associated with smaller total error scores. Such an item lacks homogeneity with the other questions about that flight parameter, and its inclusion in the test tends to weaken or, if negatively correlated with the total, run counter to measurement goals. Therefore removing or improving low and/or negatively correlated items should improve the test.

Table 8:

Item-Test Correlations (Analog Display)

Maneuver	Run	<u>Pitch</u>	<u>Ro11</u>	Heading	Airspeed	Altitude	Vertical Velocity
Climb	1 2 3 4	.291 .432 102 .194	.309 .041 .207	343 .544 .486 .113	.579 .017 .155 .437	026 .600 .261 .787	.394 ~.133 .174 .759
Climbing Turn	1	.356	.025	.200	.439	020	.223
	2	.418	.602	.384	.403	.760	.419
	3	052	.592	_	.244	100	.552
	4	.365	.550	.056	070	.269	.277
Level Turn	1	.183	.035	206	.065	.180	.229
	2	.528	.201	.405	.196	.086	.492
	3	.355	.516	.316	131	122	.387
	4	176	.215	.035	.581	061	.810
Descent	1 2 3 4	.128 .090 .346 .256	.097 .020 .448	.427 .359 .122 .241	.243 .344 .046 066	.020 032 161 093	.406 .018 .180 015
Descending Turn	1	.060	.153	352	.187	.848	.144
	2	.049	.547	031	.509	.025	138
	3	.349	.382	.345	.066	.027	.046
	4	109	.166	.040	.127	.851	.361

VII. Conclusions and Recommendations

The objective of this study was to test an STE display evaluation technique, that is, to demonstrate its validity by applying it to two ostensibly different display types and measuring the ability of IP's to recall specific flight indications shown during short flight segments of five different maneuvers, viz., climb, climbing turn, level turn, descent, and descending turn. The flight parameters representing the flight. segment included airspeed, pitch angle, roll angle, altitude, vertica! velocity, and heading. These six flight parameters were analyzed separately to determine the sensitivity of the evaluation measure to display differences. The goal was to validate the IOS display evaluation technique to determine whether it would be worthwhile for the Air Force to pursue. In light of these results, the IOS display evaluation technique described in this report deserves further attention, given that the goals of the technique in this period of its development appear to have been realized. The deficiencies which are evident are apparently not insuperable, although attention is needed in several aspects of the test.

The most logical approach to the selection of questions for the benchmark task would be to choose flight segments from a larger group of such segments to obtain a greater variety of reportable events and time intervals. Though logical, it may be uneconomical because of the large amount of flight data to be processed. The present results fall short of those ultimately sought but make the effort a worthy one within a realistic framework.

One consideration pertinent to the understanding of the present data relates to the airplane being simulated by the computer program or data base. This simulated airplane is an "educated guess" about the flight characteristics of some future extension of the A-7, referred to informally as the "Super A-7." C-130 or C-141 pilots would be expected to perform much better on a task based on an airplane with more familiar flight characteristics. It may well be necessary to have sets of questions relating to various general aircraft types so that the observers evaluating a display can be matched, in terms of current experience, to the display's intended application. Certainly, the "super performance" of the simulated airplane in this study was confusing to the MAC pilots who served in the present study.

Another aspect of the flight characteristics of the simulated airplane was the interaction of these flight characteristics with the instruments used in the analog display. For example, the strip chart recording of one flight (Climb, Run 2) shows an airspeed of 700 knots though the maximum limit for the airspeed indicator is 500. Another example is the vertical velocity indicator which reads a maximum of 5800 ft/min while vertical speeds frequently exceed this value. (Maximum values for analog instruments were used to set maximum values for the CRT digital display.) These display limitations (or airplane excessive performance) cause the evaluative power of the test to be weakened.

Another weakness in the present study had to do with the current experience of the pilots serving as observers in the study. In several instances an altitude question received a response from a C-141 pilot which was 10,000 ft. in error because he was accustomed to a tape readout rather than dial-and-needle indications.

For some pilots who are accustomed to reading roll angle (bank) indications at the bottom of their ADI, there was a tendency to read right for left and vice versa on the one used in this study which had roll indication at the top. This may account in part for the lack of significant difference between the means for analog vs. digital in the ANOVA, since in the digital mode the left-right designation is alphabetic rather than being a tilt with respect to the artificial norizon. Roll angle interacts with the type of maneuver in some fairly obvious ways; in an attempted straight climb or descent the roll angle will remain close to zero and the size of the average error for these maneuvers will be correspondingly small.

Heading recall errors were difficult to score because the magnitude of the error was not as simply defined as with altitude. For example, should an observer report the heading to be 010 degrees (as presented on the analog instrument) when it was in fact 020 degrees, the error is easily scored as 10. Likewise, a report of 170 degrees instead of the correct heading of 190 degrees is scored as an error of 20. However, if the error is a difference between a heading greater than 270 and less than 090 the magnitude of the error is numerically larger than one of the same angular difference between a heading greater than 090 and less than 270. A solution might be to measure the error as angular difference, but this approach would make no sense applied to the digital display. Since the comparison of the two display types requires comparable measures, it appeared more justifiable to score responses in terms of numerical difference than to treat the digital display responses as though it presented heading information in a way comparable to the analog instrument, i.e., the round dial and pointer.

The vertical velocity, as displayed on the round dial (analog) instrument is another potential source of unwanted variation in the data. If, in a given flight segment, the maximum upward velocity was 5000 (+5000) feet per minute and the maximum downward velocity was 4900 (-4900) feet per minute, a report regarding maximum vertical velocity of -4900 would be scored as an error of 9900 feet per minute. As a deviation from zero feet per minute of vertical velocity the error is only 100 although the algebraic difference is 9900. Of course, the same kind of error may occur with the digital display if the observer recalls a value with a negative sign when it was positive or vice versa. If a value recalled is the largest negative value while the largest value is actually positive, scoring can be based either on the basis of the difference between the absolute values or on the angular difference between reported and correct values (algebraic difference), depending on the conceptual framework used. The choice made for this study was to take the algebraic difference for questions about maximum vertical speed without the direction (up or down) being specified in the question.

Further improvement in the technique for evaluating IOS displays should start with selecting or generating flight segment tapes which have the range and variety of characteristics from which to select items corresponding to the question categories. The events to which the questions refer should be easily distinguishable from other activity in the flight segment. In the present study some events used for the questions were not as distinctly separated from other activity as may be desired.

A longer time should be devoted to making sure that each observer can read the instruments correctly and understand the kinds of questions to be asked. A response system should be developed to permit observers to perform the task without requiring the presence of someone to record data.

The need for quantitative, objective measures of quality for intelligent procurement of advanced displays has received frequent mention, but not much has been done to remedy the problems associated with the more usual haphazard, subjective selection methods. The reason for this state of affairs is probably due to the magnitude of the effort needed to produce an objective evaluation technique.

The concept of the benchmark task applied to this problem is demonstrably worthwhile. Though it may require a number of iterations before it is developed to a satisfactory level, this evaluation technique is a way out of the problems of older methods. The program should receive the continuity of attention required to maintain the momentum necessary to bring it to success.

UTBLICAKAPHA

- Donaldson, T.S. <u>Subjective scaling of student performance</u>. Rand P-45>6, March 1971.
- Engel, J.D. <u>An approach to standardizing human performance assessment.</u>

 (AD-717 258). George Washington University, Human Resources Research Organization, October 1970.
- *Evaluation of instruction. Chief of Naval Education and Training, CNTECHTRA Instruction 1540.12, 342A as of January 1975.
- **Faconti, V., Mortimer, C.P.L., & Simpson, D.W. <u>Automated instruction</u>
 and performance monitoring in flight simulator training.

 AFHRL-IR-69-29. AD-704 JZU. wright-Patterson AFB, UH: Training
 Research Division, Air Force Human Resources Laboratory, February
 1970.
 - Faconti, V., & Epps, R. <u>Advanced simulation in Undergraduate Pilot</u>

 <u>Training: Auto instructional system.</u> AFHRL-TR-70-09(LV).

 A2-AU17-165. Wright-Patterson AFB, UH: Advanced Systems Division,
 Air Force Human Resources Laboratory, Uctober 1975.
- *Finley, D.L., Robins, J.E., & Ryan, T.G. <u>Training effectiveness</u>

 <u>evaluation of naval training devices</u>. (AD-908 034). Bunker-Ramo

 Corporation, Westlake Village Electronic -- Etc., December 1972.

- *Fogel, L.J., et. al. <u>Investigation of principles of control/uisplay for</u>
 RPVs. (Ap-767 414). pecision Science, Inc., February 1973.
- *Fromer, R., Horowitz, M.W. <u>Flight information display for instructional</u> consoles. Tech. Report 20-DS, -31-1, September 1958.

- *Gopher, D., et. al. <u>The measurement of operator capacity by manipulation of dual-task demands</u>. (AD-ADU6 352). Illinois University Savoy Aviation Research Laboratory.
- Hunter, C.C. New dimensions to instruction. <u>uSAF instructors Journal</u>, 1970. 8(2)-11-15
- Enhancement of human effectiveness in system design. (AD-AUU4 149).

 Training June 1974. Illinois University Savoy Aviation Research

 Laboratory.
- The impact of full mission simulation of the TAC comoat crew training system. (AD-B004 457L). Air war College, Maxwell AFB, Alabama, April 1975.
- **Kanarick, A.F., et. al. Effects of value on the monitoring of multichannel displays. Human Factors, 1969, Vol. 11.
 - *Man The focus of the training system. (Au-768 756). Proceedings of the Naval -- Etc., Naval Training Equipment Center, Urlango, Florida,

 November 1973.
 - McGratn, J., & Harris, D. (Eds.) <u>Adaptive training aviation research</u>
 monographs. Inst. of Aviation, university of illinois, August 1971.
- *Miller, G.G. <u>Some considerations in the design and utilization of simulators for technical training</u>. AFHRL-TR-74-65, AD-ADD1-65D. Lowry AFB, CO: Technical Training Division, Air Force Human Resources Laboratory, August 1974.
- Miller, R.L. <u>Techniques for the initial evaluation of flight simulator</u>

 <u>effect</u>. (AD-A036 460). wright-Patterson AFB, UH: Air Force

 Institute of Technology, December 1976.

- *Pearlstein, R.B., Schumacher, S.P., Rifkin, K.E. <u>Information uispla</u> guide. Valencia, PA: Applied Sciences Association, Inc., 1974.
- Preliminary gound instructor's pilot manual. Naval Air Systems Command,
 Displays and Depriefing Subsystem (DDS). Air Compat Maneuvering
 Range, (Second Edition, Johns Hopkins University, Silver Springs,
 1975).
- **Price, H.E. <u>Human engineering recommendations for the instructor</u>

 pilot's station of the ASJ-1 weapon system trainer. (AD-678-371 and

 370). Report PRA-36-15, September 1936.
- *Prophet, W.W., Caro, P.W., Hall, E.R. <u>Some current issues in the design</u>
 of flight training devices. (AD-743 Z7U). Alexandria, VA: Human
 Resources Research Organization, 1971.
 - Rose, H.C. A plan for training evaluation. <u>Training and Development</u>
 Journal, 1968.
- *Ryan, L.E., Puig, J.A., & Micheli, G.S. <u>An evaluation of the training effectiveness of device 2F90</u>. (AD-750 248). Naval Training Equipment Center, Orlando, Florida, August 1972.
- Shipley, B.D. <u>Measurement of flight performance in a flight simulator</u>.

 AD-ADD4 488. Report No. TR-4083U, Arizona State University,

 Education Department.
- Snipley, 8.D. An automated measurement technique for evaluating pilot skill. (AD-AU33 92U). Arizona State University, Tempe College of Education, February 1976.
- Smode, A.F. Human factors inputs to the training device design process. NAVTRADEVUEN 69-U-0298-1. NTEC, 1971.

- **Smode, A.F. Recent developments in instructor station design/utilization for flight simulators. Human Factors, 1974, Vol. 16.
- *Smode, A.F., Lam, K.D. (Eds.) <u>Proceedings of the Conference on Military</u>
 Instructor Training in Transition. TALL Report No. 25, May 1975.
- Stanley, M.u. A Methou for Developing a Criterion for Compat Performance. (AD-765-679). Monterey, CA: Naval Postgraduate School, June 1975.
- *Swain, A.D. <u>Guide for the design and evaluation of the instructor's</u>

 station in training equipment. wADU-TK-04-064, AD-72 lub. December
 1954.
- Synthetic trainer instructor's guide. Fort Rucker, AL: U.S. Army Aviation School, Movember 1969.
- of altitude displays. (AU-752 729). ASU, SPAFB, August 1972.
- **Tyler, D.M., et. al. Monitoring performance across sense modes an individual difference approach. Human Factors, 1972, vol. 14.
- **Valverue, H.H. A review of flight simulator transfer of training studies. Human Factors, 1975, 10(6).
- *Wheaton, G.R., Mirabella, A., & Farina, A.J. <u>Trainee and instructor task</u>

 <u>qualification: Development of quantitative indices and a predictive</u>

 <u>methodology</u>. Durin, Dunlap & Association, Inc., January 1971.
- Weyer, D.C., & Fuller, J.H. <u>Development of a syliabus and</u>

 <u>student/instructor guide for use with a full mission simulator.</u>

 AFHRE-TR-76-9U, AU-AU2/ 52L. Williams AFB, AZ: Flying Training Division, Air Force Human Resources Laboratory, December 1976.
- Young, F.E. <u>Concept formulation report, synthetic training system.</u>

 (AD-675 505). Falls Unuren, VA: Melpar, Inc., April 1966.

**Zipoy, D.R., et. al. <u>Integrated information presentation and control</u>

<u>system study</u>. AFFDL-TR-70-79, Vol. I through IV, July 1970 to

January 1973.

APPENDIX A: INSTRUCTIONS TO SUBJECTS

You have been asked to take part in a research project aimed at development of evaluation techniques for flight simulator instructor/operator displays. It is to be noted that the displays which you will be viewing are not under evaluation nor do they represent the state of the art in display technology. These displays are merely vehicles for testing the evaluation method under consideration.

A series of short flight segments were flown in a flight simulator and recorded. These recorded data will be played back to you on two different displays - analog flight instruments and digital CRT. After viewing each flight segment you will be asked to respond to a set of questions concerning the displayed data. Basically, we are trying to determine if this method can be used to ascertain the relative efficacy of alternative displays for providing different types of information to the instructor located at a remote station. Keep in mind it is this method for determining the power of the display, to provide certain types of information under certain conditions, which is under evaluation and not your individual powers of observation. It is, in fact, hoped that observers are more alike than different in their powers of observation and that individual differences will prove to be insignificant.

The questions will be of four types categorized on the basis of the kind of memory task implied. For example, the question may relate to the extreme values of a given flight parameter the answer to which requires retention of display contents over the entire flight segment. Such a

question may be worded in the following way: "What were the extremes of airspeed during the flight segment?" The question concerns a range of values over an extended period of time.

A second type of question deals also with a range of values but refers to a particular point in the maneuver, e.g., "What was the change in airspeed in the transition to level off:" The answer requires the naming of two values, one displayed just before transition to level-off was started, another after it was completed.

The third and fourth types of question ask for single specific values rather than ranges. Like the first type, the third kind of question applies to the entire flight segment, e.g., "What was the highest airspect during the flight segment?" (This particular question is implied in the first question about extremes of airspeed.)

The fourth type of question is like the second type in that it asks for display content at some particular point in the flight segment and like the third type in that a single specific value is requested.

The average duration of the flight segments is a little less than 2-1/2 minutes. They will represent five basic flight maneuvers: straight climb, climbing turn, level turn, straight descent, and descending turn.

The flight indications displayed will most probably not be representative of aircraft with which you are familiar since the computer program was designed to simulate a developmental high performance aircraft.

You will be asked questions after each flight segment on each of six fligh parameters: pitch, roll, heading, vertical velocity, altitude, and bearing

APPENDIX B: TEST CONDITIONS AND RAW DATA

WSTPUCTOR/OPERATOR STATION - DISPLAY EVALUATION STUDY - TABULATIUN OF RESPONSES

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APPENDIX C: TEST QUESTIONS

F1 t.	Flt. 1 and 21 (Case 1, Run 1 - 140 sec.)			
Ques.		Ques. Type	Correct Responses	From Start (Seconds)
2 -	Lithat ware the extremes of pitch angle?	(1)	-2 degrees	120
5.	What was the change in roll angle from the start of the flight segment to the point where the wings were leveled	(2)	+32 degrees -2 degrees +1 degree	19 38
رب، ا	for the rest of the figure: What was the maximum numerical value of <u>heading</u> ?	(3)	015 degrees	
4	What was the initial airspeed?	(4)	215 knots	 1
		(1)	4,953 feet 19,523 feet	22
6.	What was the vertical speed change at the start of the climb? (2)	(2)	+480 ft/min +5,800 ft/min	20 36

CLIMB (continued)

Flt. 2 and 22 (Case 1, Run 2 - 140 sec.)

Ques. No.		Ques. Type	Correct Responses	Time From Start (Seconds)	•
1.	What were the highest and lowest pitch angles in the first 30 seconds of the climb?	(2)	+30 degrees 0 degrees	9 23	
5,	What was the largest value of <u>roll angle</u> and was it right or left?	(3)	-5 degrees	91	
ë.	What was the minimum numerical value of <u>heading</u> just before level off?	(4)	264 degrees	115	
4.	What were the extremes of <u>airspeed?</u>	(1)	106 knots 500 knots	10 63	
5.	What range in altitude fluctuation occurred prior to when a consistent climb was started?	(2)	2,203 feet 2,500 feet	9	
<i>•</i>	What was the highest value of vertical descent speed?	(3)	-2,340 ft/min	4	

Flt. 3 and 23 (Case 1, Run 3 - 180 sec.)

Ques.	S.	Ques. Type	Correct Responses	Time From Start (Seconds)
٦.	What was the highest pitch angle during the segment?	(3)	+26 degrees	51
2.	What was the roll angle in the last part of the climb?	(4)	0 degrees	52
m 63	What were the extreme <u>heading</u> values in the segment?	(1)	697 degrees 097 degrees	1 180
4.	What was the change in airspeed in the 20 seconds prior to level-off?	(2)	350 knots 350 knots	115 135
5.	What was the minimum altitude?	(3)	3,600 feet	r
9.	What was the high point in vertical speed reached when the nose was raised in the climb?	(4)	+5,800 ft/min	51

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Ċ	Ques.	Ques.	Correct	From Start (Seconds)
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•	 What was the lowest <u>pitch angle</u> in the last third of the climb portion of the segment? 	(4)	+3 degrees	86
2	2. What were the extremes of right and left roll angle in the segment?	(1)	-7 degrees +6 degrees	50 52
თ 64	 What change in heading occurred on the initiation of the climb? 	(2)	350 degrees 350 degrees	25 25
•	Mhat was the highest air_peed?	(3)	362 knots	110
ų)	5. What was the altitude just prior to the marked climb portion of the segment?	(4)	15,000 feet	25
9	6. What were the extremes of <u>vertical speed?</u>	(1)	-120 ft/min +5,800 ft/min	55

CLIMBING TURN

Flt. 5 and 25 (Case 2, Run 1 - 140 sec.)

Ques.		Ques. Type	Correct Responses	Time From Start (Seconds)
;	What were the extremes of pitch angle?	(1)	+2 degrees +11 degrees	17 56
2.	What was the change in <u>roll angle</u> as the turn was initiated?	(2)	0 degrees +34 degrees	2 4 28
ë.	What was the lowest numerical value in <u>heading</u> indications throughout the flight segment?	(3)	030 degrees	25
4.	What was the <u>airspeed</u> after level-off?	(4)	353 knots	115
	What were the extreme altitude indications in the flight segment?	(1)	15,143 feet 20,040 feet	20 140
9.	What was the initial change in <u>vertical speed</u> at the beginning of the maneuver?	(2)	-600 ft/min +900 ft/min	15 17

CLIMBING TURN (continued)

F1t.	Flt. 6 and 26 (Case 2, Run 2 - 150 sec.)			į
Ques. No.	•	Ques. Type	Correct Responses	From Start (Seconds)
-:	About half a minute before the end of the segment the pilot lowered the nose and then brought it up again before coming down with it to level-off. How low and how high did the pitch angle go in this portion of the flight segment?	(2)	+4 degrees +8 degrees	33
2.	What was the maximum roll angle?	(3)	+29 degrees	27
κ'n	What was the <u>heading</u> at the beginning of the flight segment?	(4)	016 degrees	25
4.	What were the extremes of airspead?	(1)	214 knots 283 knots	34 150
က်	What was the altitude change associated with the low pitch angle which occurred in the first half of the flight segment?	(2)	16,300 feet 15,500 feet	45 60
9.	What was the maximum vertical speed?	(3)	+5,800 ft/min	67

CLIMBING TURN (continued)

Flt. 7 and 27 (Case 2, Run 3 - 150 sec.)

Ques.		Ques. Type	Correct Responses	Time From Start (Seconds)
1.	What was the highest <u>pitch angle</u> throughout the flight segment?	(3)	+13 degrees	35
2.	What was the maximum roll within the first 10 seconds after initiation of the Turn?	(4)	+30 degrees	33
ب	What were the highest and lowest <u>heading</u> indications?	(1)	360 degrees 001 degrees	100
⊄ .	What was the change in <u>airspeed</u> in the transition from climb to level-off?	(2)	350 knots 330 knots	130 140
5.	What was the lowest altitude in the segment?	(3)	15,150 feet	1
	What was the high <u>vertical speed</u> at the beginning of the climb?	(4)	+5,800 ft/min	36

CLIMBING TURN (continued)

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25	Ųν⊢s. No.	Oues. Type	Correct Responses	Time From Start (Seconds)
1	What was the low pitch angle just before level off?	(4)	-4 degrees	119
2.	What were the extremes of <u>roll?</u>	(1)	+9 degrees -33 degrees	79 84
რ 68	What was the <u>heading</u> change in the first half of the flight segment?	(2)	088 degrees 042 degrees	11 76
	What was the lowest airspeed in the segment?	(3)	303 knots	37
5.	What was the starting altitude?	(4)	15,200 feet	1
ιά	What were the extremes of <u>vertical speed?</u>	(1)	45,800 ft/min -5,800 ft/min	46 119

Flt. 9 and 29 (Case 3, Run 1 - 130 sec.)

Ques.		Ques. Type	Correct Responses	Time From Start (Seconds)
-	What were the extremes of <u>pitch angle</u> during the flight segment?	(1)	+7 degrees +3 degrees	47 76
2.	What was the change in roll angle in the first five seconds as the turn was initiated?	(2)	O degrees +37 degrees	15 18
<i>ش</i>	What was the highest numerical indication of <u>heading</u> in the segment?	(3)	360 degrees	85
4	What was the airspeed at the end of the flight segment?	(4)	275 knots	130
5.	What were the extremes of altitude?	(1)	19,811 feet 20,410 feet	20 130
6.	What was the change in <u>vertical speed</u> on roll-out?	(2)	+1,200 ft/min 0 ft/min	108 120

LEVEL TURN (continued)

Flt. 10 and 30 (Case 3, Run 2 - 160 sec.)

Ques. No.		Ques Type	Correct Responses	Time From Start (Seconds)
1.	Shortiy before the halfway point the nose comes down to a low point and then pitches up. What were the low and high pitch angles in this portion of the flight segment?	(2)	-1 degree +7 degrees	70 32
۲:	What was the maximum roll to the right?	(3)	+33 degrees	29
3.	What was the final neading?	(4)	280 degrees	160
4	What were the extremes of airspeed in the segment?	(1)	236 knots 261 knots	80
ທ່	There was a low point in <u>altitude</u> about 30 seconds prior to roli cut. What change was there between this point and the end?	(2)	20,026 feet 20,200 feet	128 160
. 9	What was the greatest vertical speed attained?	(3)	-3,420 ft/min	71

LEVEL TURN (continued)

Flt. 11 and 31 (Case 3, Run 3 - 200 sec.)

Ques.		Ques. Type	Correct Responses	Time From Start (Seconds)
, mi	What was the lowest pitch angle in the segment?	(3)	0 degrees	131
2.	What was the maximum roll in the first ten seconds after the initiation of the turn?	(4)	+24 degrees	23
in,	what were the highest and lowest <u>heading</u> indications?	(1)	130 degrees 310 degrees	19 178
4	What was the change in airspeed in transitioning from the bank to wings-level flight?	(2)	270 knots 270 knots	74 85
5	What was the highest altitude in the flight segment?	(3)	20,104 feet	26
6.	What was the high <u>vertical speed</u> associated with the high pitch angle at the start of the turn?	(4)	+1,500 ft/min	24

LEVEL TURN (continued)

Flt. 12 and 32 (Case 3, Run 4 - 190 sec.)

Gues. No.		Ques. Type	Correct Responses	Time From Start (Seconds)	
1.	About two-thirds the way through the flight segment the airplane pitched up briefly. What was the highest pitch angle in this portion of the flight segment?	(4)	+8 degrees	128	
2.	What were the extremes of <u>roll?</u>	(1)	-33 degrees +15 degrees	161 171	
m	What was the <u>heading</u> change in the last 25 seconds of the flight segment?	(2)	305 degrees 310 degrees	165 190	
4.	What was the maximum airspeed in the segment?	(3)	292 knots	95	
5.	What was the initial altitude?	(4)	20,300 feet -1,680 ft/min	1	
9	What were the extremes of vertical speed?	(1)	+2,400 ft/min	128	

F1#.	Fit. 13 and 32 (Case 4, Kun 1 - 120 Sec.)			1 ime
Ques.		Ques. Type	Correct Responses	From Start (Seconds)
2	What were the extremes of <u>pitch angle</u> during the flight	(1)	+5 degrees	22 34
~i	Segment: What change in <u>roll</u> occurred in the transition from level flight to descent?	(2)	0 degrees 0 degrees	C C C C C C C C C C C C C C C C C C C
مري	What was the lowest numbered heading indication?	(3)	012 degrees	120
. 7	What was the airspeed just before the start of level-off?	(4)	315 knots	105
. v	What were the extremes of altitude in the segment?	(1)	20,001 feet 15,253 feet	3 120
9	What was the change in vertical speed in the transition from descent to level-off?	(2)	-3,600 ft/min O ft/min	107 120

DESCENT (continued)

Flt. 14 and 34 (Case 4, Run 2 - 115 sec.)

Ques. No.		Ques. Type	Correct Responses	Time From Start (Seconds)
.;	Starting from an initial <u>pitch angle</u> in level flight, the nose was brought down, then up, prior to lowering it for the descent. What was this initial pitch change?	(2)	0 degrees +9 degrees	20 24
ا 2	What was the maximum roll to the left in the descent?	(3)	0 degrees	115
	What was the heading just prior to the start of the descent?	(4)	050 degrees	22
4.	What were the extremes of <u>airspeed</u> in the segment?	(1)	284 knots 338 knots	28 63
ų,	What was the increase in altitude just prior to the descent?	(2)	20,000 feet 20,190 feet	21 29
9.	What was the highest vertical speed upward?	(3)	+3,300 ft/min	25

DESCENT (continued)

ز. نا	F15. 15 and 35 (Case 4, Run 3 - 110 sec.)			
				Time
Ques.		Ques. Type	Correct Responses	From Start (Seconds)
2	What was the lowest pitch angle in the flight segment?	(3)	-9 degrees	27
5	What was the roll angle just before level-off?	(4)	+1 degree	95
က်	What were the highest and lowest heading indications?	(1)	195 degrees 199 degrees	56 110
4.	What was the change in airspeed in the transition to level-off?	(2)	245 knots 280 knots	86 110
ι,	What was the minimum altitude?	(3)	15,497 feet	72
.	What was the greatest downward vertical speed just before level off?	(4)	-3,000 ft/min	26

DESCENT (continued)

F1 t.	Flt. 16 and 36 (Case 4, Run 4 - 110 sec.)			Time
Ques.		Ques. Type	Correct Responses	From Start (Seconds)
<u></u>	Upon initiation of the descent the nose is first pitched up. What was the highest <u>pitch angle</u> in this part of the flight segment?	(4)	+7 degrees	17
2.	What were the extremes of roll in the segment?	(1)	+12 degrees -9 degrees	23 47
ë.	What neading change occurred in the transition from descent to level-off?	(2)	285 degrees 285 degrees	96 95
4	What was the highest airspeed in the segment?	(3)	329 knots	7.7
5.	What was the final altitude?	(4)	15,180 feet	111
6.	What were the extremes of vertical speed?	(1)	+1,200 ft/min -5,800 ft/min	17 85

DESCENDING TURN

Flt. 17 and 37 (Case 5, Run 1 - 132 sec.)

Ques. No.		Ques. Type	Correct Responses	Time From Start (Seconds)
1.	What were the extremes of pitch angle in the flight segment?	(1)	+4 degrees -4 degrees	1 36
2.	What was the change in roll within the first ten seconds after the initiation of the turn?	(2)	0 degrees -29 degrees	23 28
w.	What was the <u>heading</u> just prior to the initiation of the descent?	(3)	007 degrees	20
4	What was the starting airspeed?	(4)	300 knots	-
က်	What were the extremes of altitude?	(1)	20,002 feet 15,353 feet	3 132
9	What change occurs in <u>vertical speed</u> in the first third of the flight?	(2)	0 ft/min -4,550 ft/min	17 36

DESCENDING TURN (continued)

Flt. 18 and 38 (Case 5, Run 2 - 170 sec.)

Ques.	5.	Ques. Type	Correct Responses	Time From Start (Seconds)
- i	What was the change in pitch angle in the transition from descent to level-off?	(2)	-3 degrees +3 degrees	43
2.	What was the maximum roll to the left?	(3)	·20 degrees	153
ب	What was the final heading?	(4)	250 degrees	170
4	What were the extremes of <u>airspeed?</u>	(1)	249 knots	20
က်	What increase in <u>altitude</u> occurred before the descent?	(2)	310 knots 20,000 feet 20,280 feet	12 22
9	What was the greatest <u>vertical speed</u> in the segment?	(3)	-5,800 ft/min	37

DESCENDING TURN (continued)

Flt. 19 and 39 (Case 5, Run 3 - 120 sec.)

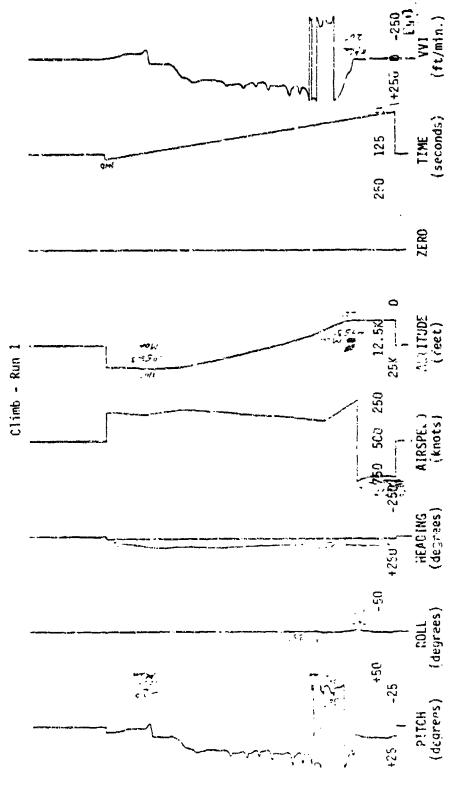
Ques.	S.	Ques. Type	Correct Responses	Fime From Start (Seconds)
-	What was the lowest <u>pitch angle</u> in the flight segment?	(3)	-6 degrees	39
2.	What was the maximum roll to the right in the first twenty seconds after initiation of the turn?	(4)	+29 degrees	31
	What were the highest and lowest <u>heading</u> indications?	(1)	170 degrees 250 degrees	15 120
4.	What was the change in <u>airspeed</u> from its peak value to its final value?	(2)	389 knots 340 knots	88 120
5.	What was the lowest altitude in the segment?	(3)	15,207 feet	119
9.	What was the greatest <u>vertical speed</u> in the first third of the segment?	(4)	-5,800 ft/min	39

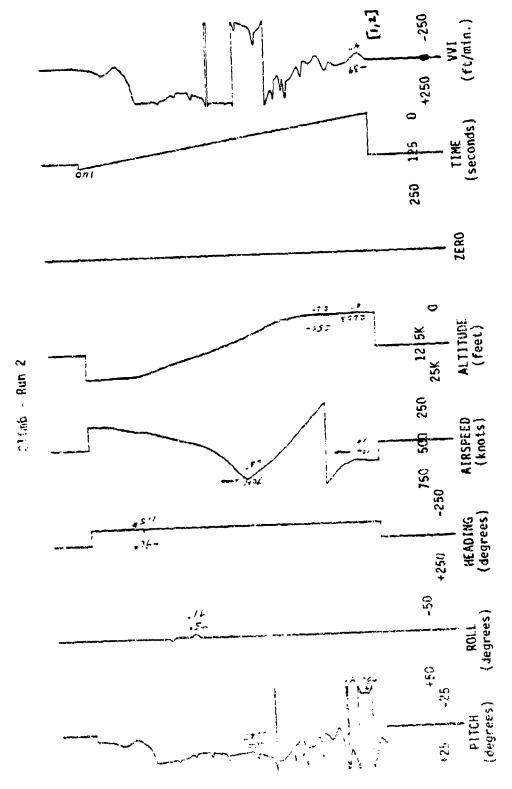
DESCENDING TURN (continued)

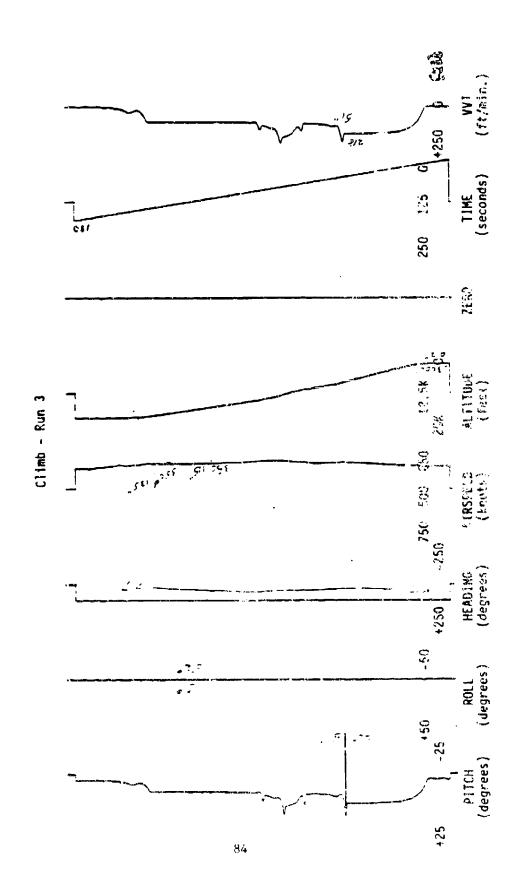
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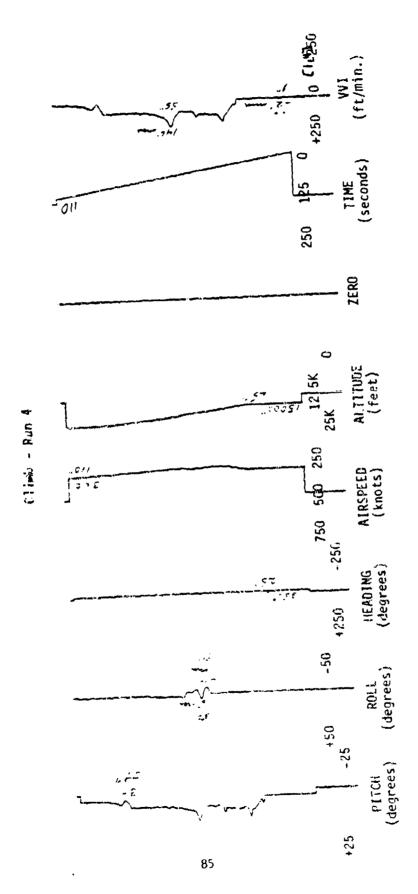
	F1t.	Fit. 20 and 40 (Case 5, Run 4 - 170 sec.)		
	Ques.		Ques. Type	Correct Responses
	1.	What was the lowest <u>pitch</u> angle just piror to level off?	(4)	-4 degrees
	2.	What were the extremes of <u>roll</u> in the segment?	(1)	-32 degrees +11 degrees
UΛ	ب	What change in heading occurred during the last 30 seconds of the flight segment?	(2)	120 degrees 120 degrees
	4.	What was the maximum <u>airspeed</u> ?	(3)	325 knots
	5.	What was the starting altitude?	(4)	20,002 feet
	9	What were the extremes of <u>vertical speed</u> in the segment?	(1)	-5,800 ft/min +840 ft/min

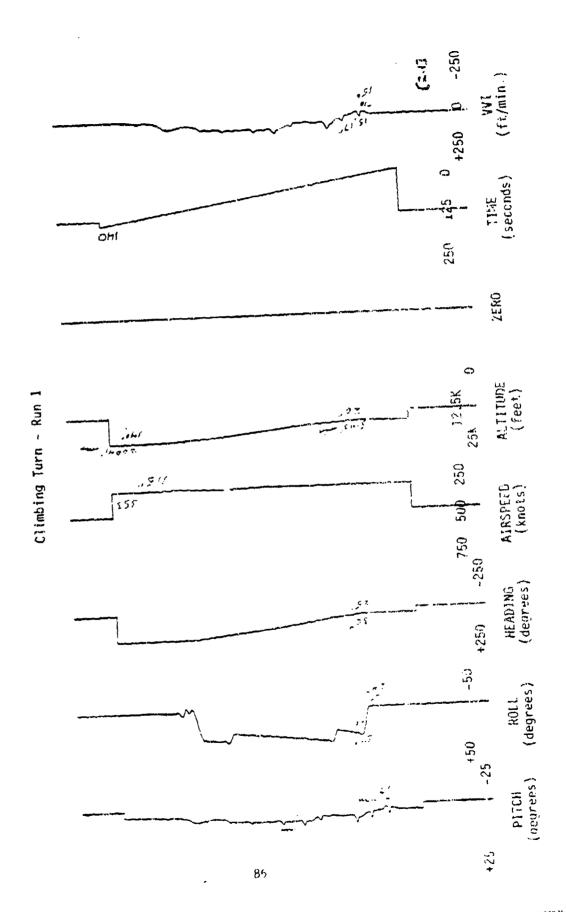
APPENDIX D: STRIP CHART RECORDINGS OF THE SIX FLIGHT PARAMETERS

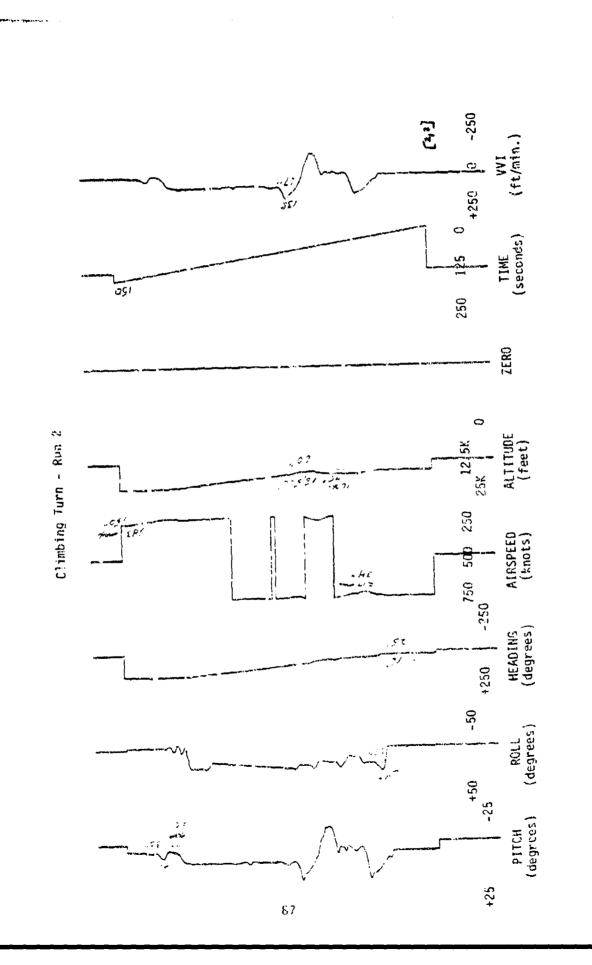


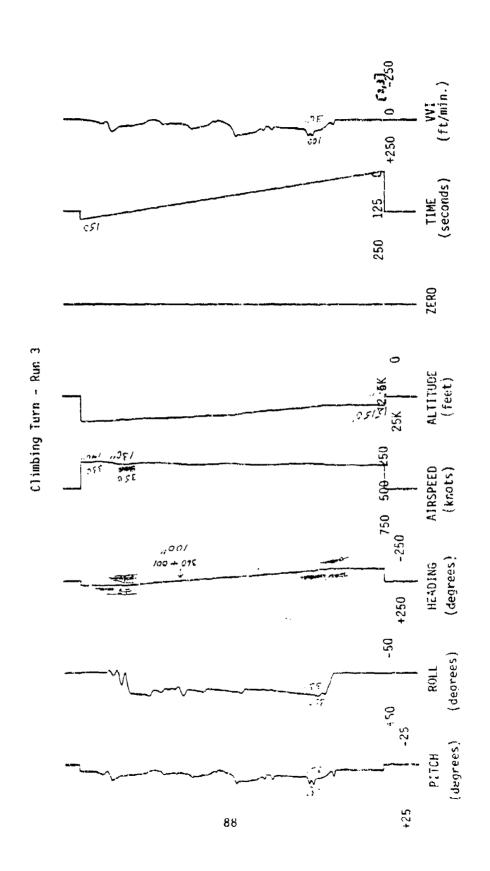


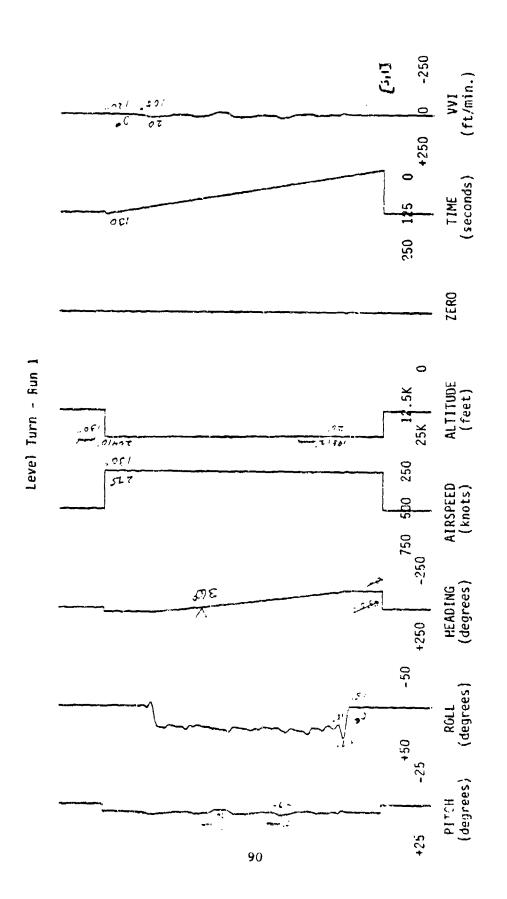


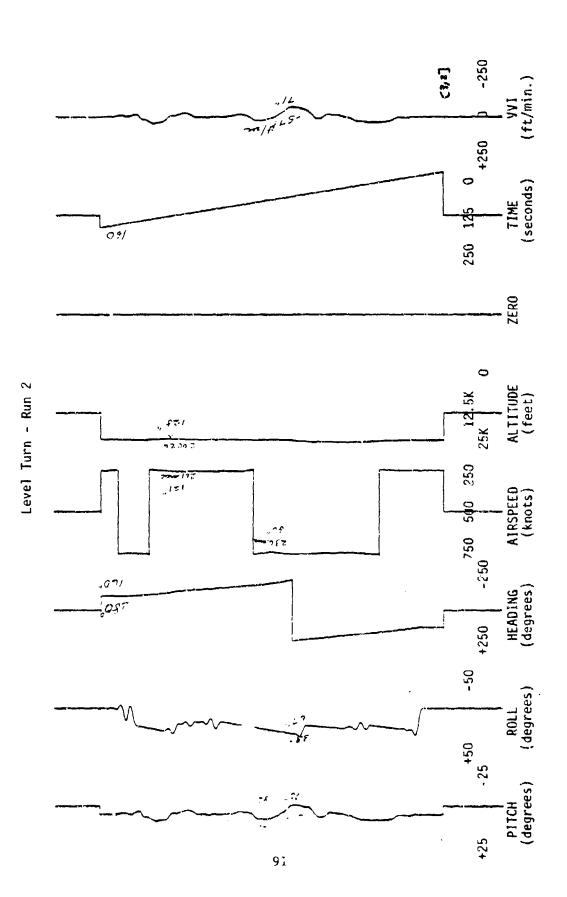


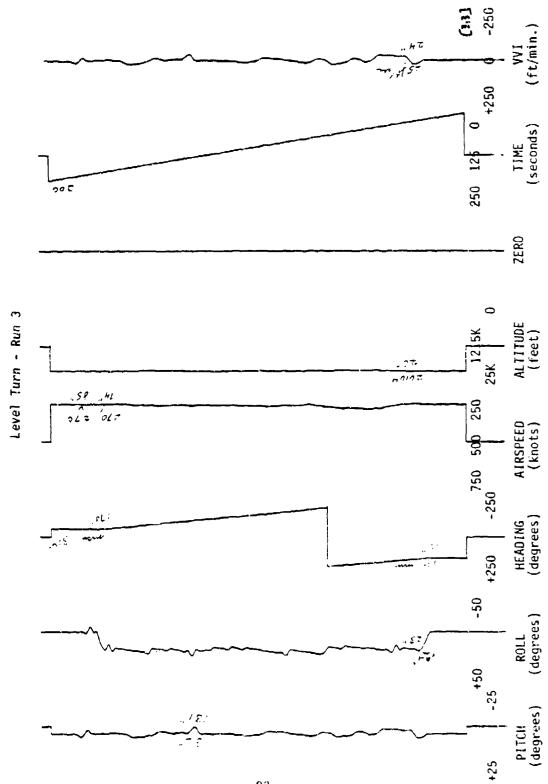


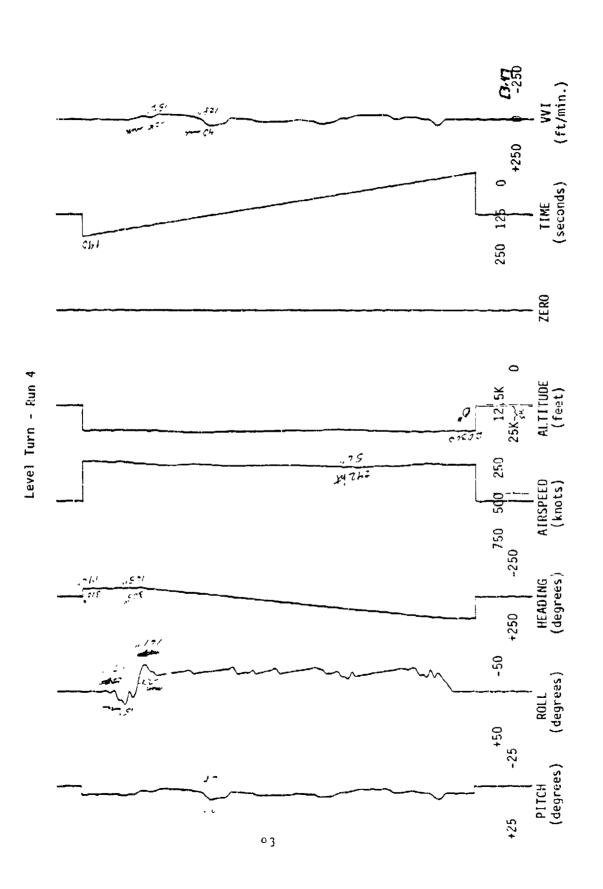


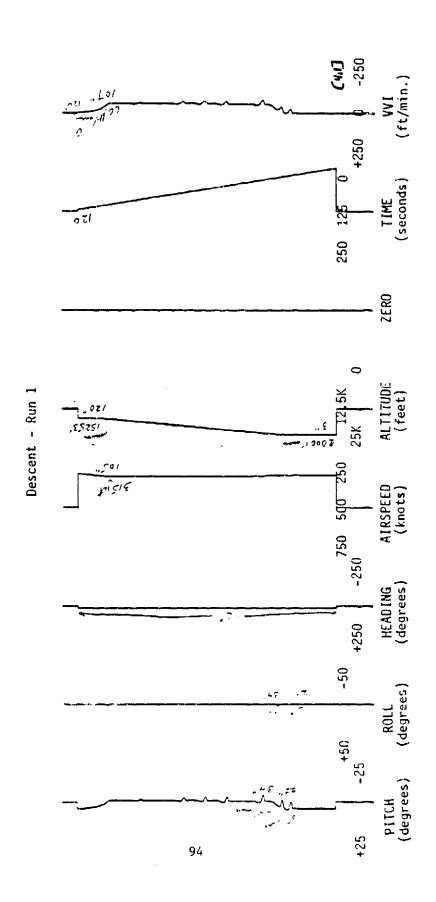




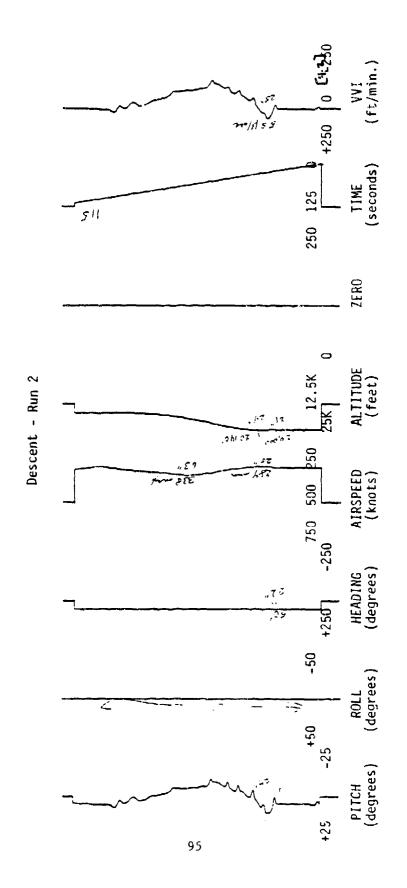


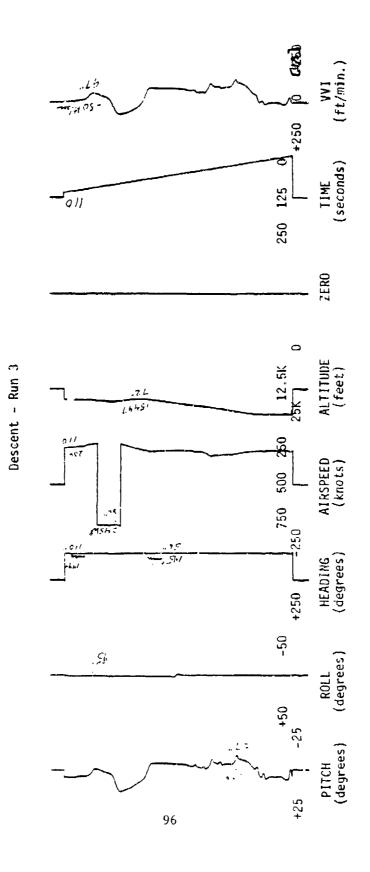


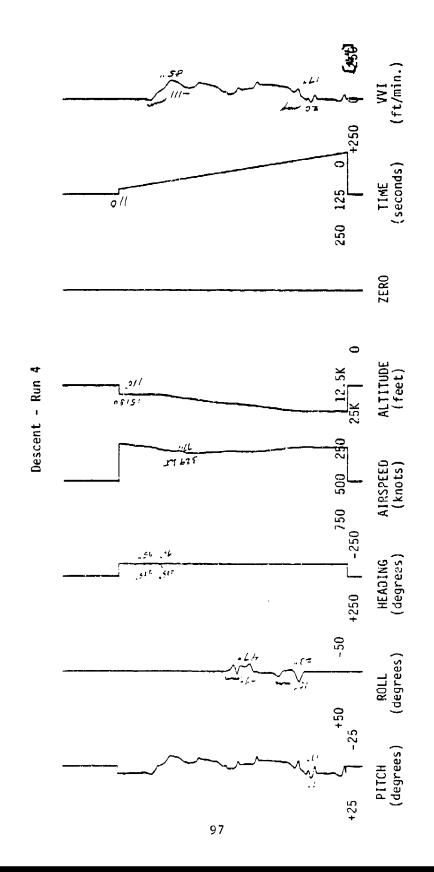


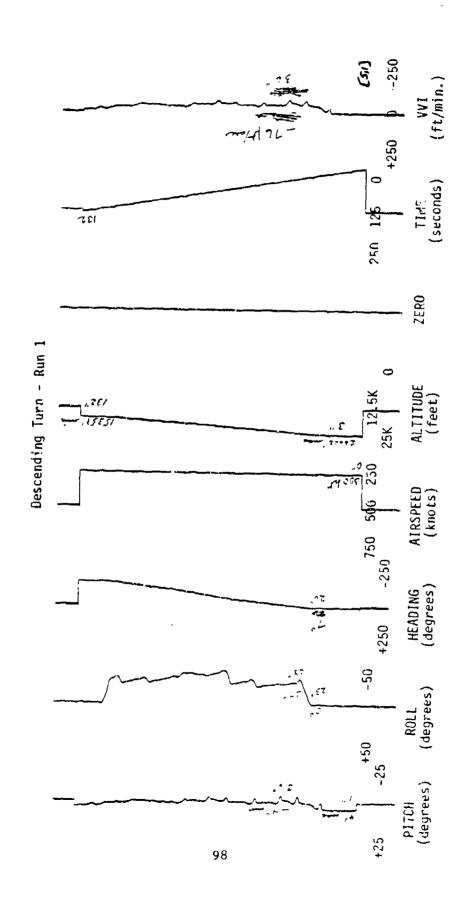


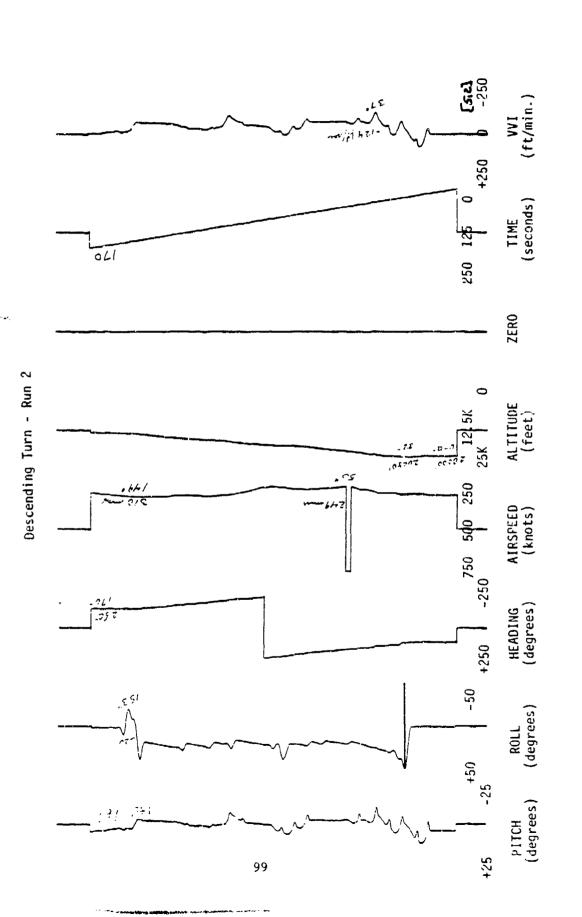
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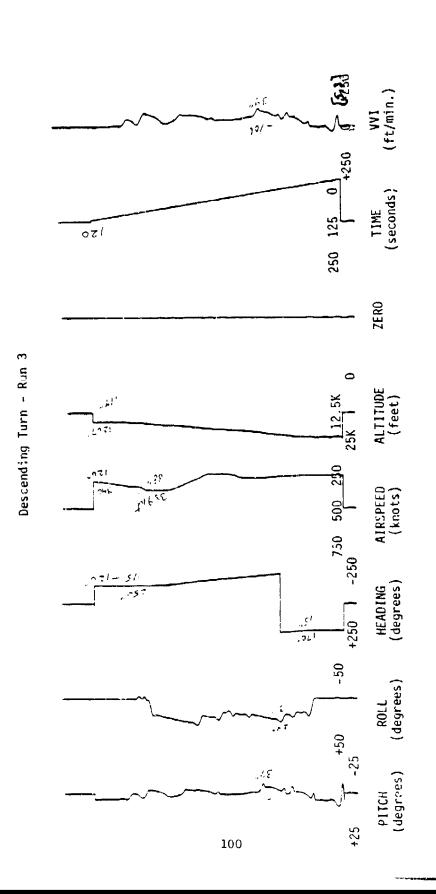


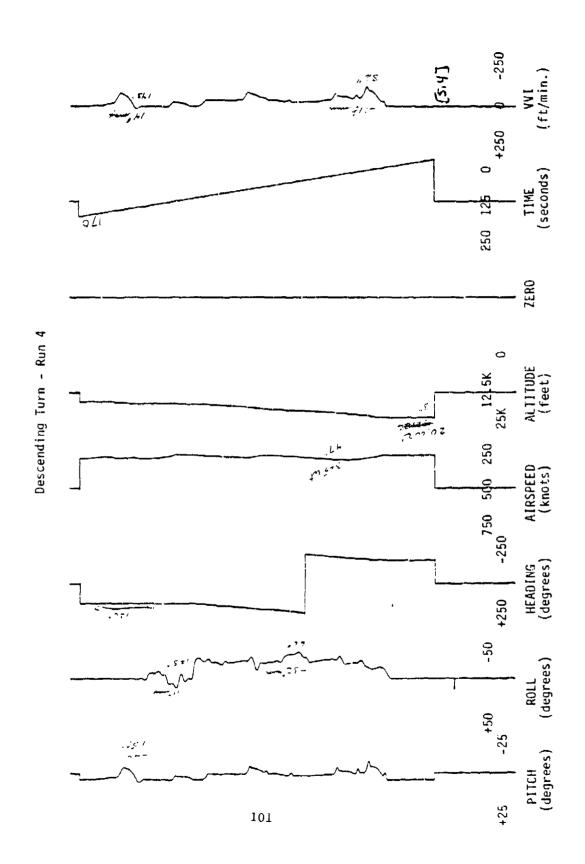












APPENDIX E: FRESENTATION ORDER FOR FLIGHT SEGMENTS AND QUESTIONS

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APPENDIX F: OBSERVER PILOT INFORMATION FORM

Pilot #			
Date			
Name	Rank	Age	
Total Flight Hours	-		
Present Equipment	Flt.	Hrs.	
Hours In Other Equipment	Type		
	Туре		
-	Туре		
Comments:			
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APPENDIX G: INITIAL EXPLURATURY STOLY

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Charles Elworth
Winifred Lee

Boeing Aerospace Company

Logistics Support and Services Division

Seattle, washington 90124

I. INTRUDUCTION

The purpose of this initial study was to develop and implement a recommended method of evaluating alternative display formats for use in the instructor/operator station of a flight simulator. The work included conducting a brief literature survey, analyzing the instructor's job, and developing a good approach to display evaluation. Our approach centered around developing a benchmark task that exercises many of the skills used by an instructor; developing ways to measure a subject's performance of that task; and using the derived measurement method experimentally to infer the effectiveness of a given display format.

The following sections document this work and present conclusions and recommendations. Important refinements of the method were then performed, and a more comprehensive test and demonstration of the method was conducted as a second study and is documented in the main body of the report.

11. LITERATURE SEARCH

we began with a literature survey to determine the current capacilities and knowledge regarding man-machine system performance in training systems. In particular, we selected and reviewed 50 documents pertaining to human-monitoring behavior, performance measurement/evaluation techniques, LRI graplay systems and number factors

primarily focused on the abstracts and, where appropriate, summaries. In general, most reports reviewed dealt with analysis, evaluation, design, and development of flight simulator systems and subsystems. Typically, emphasis focused on wide angle visual systems, complex motion platforms, sophisticated CRT cockpit displays and drew interfaces. Research relative to the functions and interfaces for the instructor was virtually nonexistent. (It would appear that the design of the instructor consoled has been dictated by simulator design rather than by instructor functions and information requirements.)

Of the 50 abstracts reviewed, Zo appeared to contain information applicable to this research. We ordered complete documentation for these works and reviewed them in more detail. These Zo reports are indicated by asterisks in Appendix H.

The second level of examination focused on identification of those documents with specific application to this program. Through this examination, we identified 1' documents (indicated by double asterisks in Appendix H) that were useful to the program and analyzed them in greater detail. This analysis identified the technology category of applicability (man/machine systems, task/workload, display systems, performance measurement, and performance evaluation), produced abstracts of study scope, and summarized primary study techniques used, salient input/output parameters, special capabilities and limitations and areas

of program applicability. The results of this review are summarized in Appendix 1.

In general, although data were available which applied to many issues requiring consideration in the conduct of this study (such as task analysis, man/machine task allocation, advanced display technology, and operator performance evaluation), no data were available relative to the development of methodologies that could be used to quantitatively compare the relative merits or deficiencies of one display system with another. However, the literature review did prove useful in establishing an understanding of the potential technical problems and in reinforcing our knowledge that this effort would be exploratory in nature.

III. INSTRUCTUR PILUT JUB ANALYSIS

To determine candidate maneuvers that could be used in benchmark task approach to the evaluation of IUS displays, we conducted a drief analysis of the role and duties of the simulator IP. This analysis addressed (1) IP duties, (2) IP tasks and skills, and (3) IP information requirements. Analysis methodology as well as results are discussed in the following paragraphs.

IP Duty Analysis

We identified the overall duties of a typical remotely located IP, monitoring and controlling student performance in a simulator, and categorized them as follows: simulator set-up, problem set-up, system/student performance monitoring and assessment, communicate/monitor programs, on-line/off-line depriefing, and altering or adapting the training problem depending on the student pilot's performance. The relationship of the aforementioned IP duties are illustrated in Figure G-1.

As the operator of the simulator (set up simulator), the LP is expected to check the system to insure that it is ready for the training session to be undertaken at that time. This may involve the removal of some conditions left over from a previous flight, coordinating with the software control operator, as well as testing and validating operability of the systems and its components.

In setting up the problem the IP must prepare inputs required to properly initiate the system as well as convey to the trainee what is expected of him. The amount of interaction between the IP and trainee(s) depends on the qualification and experience of the trainee and the level of difficulty of the task to be trained. Thus, even though the overall duty of the IP remains the same, the amount of time and the level of detail of interaction can vary significantly.

Monitoring of simulator functioning should be performed by the system

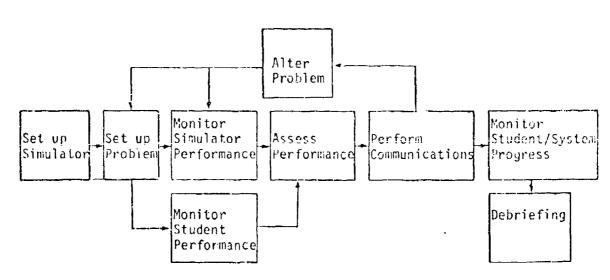


Figure G-1. Typical Instructor Duties

operator; however, the IP is quite often required to perform this function merely because his activity overlaps with that of the operator. Also, for reasons of continuity or to minimize delay, the IP will in many instances, automatically monitor the system functions even though he is not required to do so. Though this activity does not usually require excessive IP time or attention, it could be a significant consideration during heavy task loading and multi-cockpit monitoring situations.

The task of monitoring student or trainee performance demands the primary attention of the IP. He is both the certifier and diagnostician. Instructor efficiency depends on the capacility to detect indications of student performance. Such indications are the logical basis for his assessment of student performance of the trainee, and the IP's duty will vary. In retraining, the instructor will be required to alter the problem, communicate with the trainee and/or support personnel and determine the effectiveness of the remedial measures taken. If the trainee's performance is satisfactory, then the task of the IP is greatly simplified; he merely monitors the student's performance to verify that it continues to be satisfactory and prescribes new material or higher levels of difficulty.

IP Tasks and Skills

For the purposes of this study, we developed an operational scenario

upon which the IP's task and skill analysis was performed. The operational mission selected represented a typical air-to-ground mission emphasizing the terminal penetration and attack phase. We selected this phase since it involved a variety of activities (in the context of monitoring student/system performance) that require the IP to utilize various processes, skills, and content of information presented.

The functions of the terminal havigation and attack phase include (a) monitor simulator performance, (b) havigate, (c) search for and acquire target, (d) prepare for attack, and (e) deliver weapon. Within each function, we identified tasks that needed to be performed by the student pilot. We then examined each of the pilot's tasks from the viewpoint of the IP as a monitor and evaluator of the student pilot's performance of that task. With the exception of monitoring the simulator function, the tasks for the student were found to be quite different from those of the IP in that the former primarily involve physical actions such as activate, insert, etc., and the latter primarily involve mental actions such as observe, decide, verify, etc. We used the identified IP tasks as the basis upon which to generate specific information required as well as display options that are currently available. Results of that analysis are shown in Table G-1.

Specific skills the instructor must have to carry out these tasks are varied. The type of tasks performed by the LP and their relationship to the process used and the typical behavior or skill required are depicted

Table G-1. Task Analysis Summary

FUICTION	PILOT TASKS	IMSTRUCTOR TASKS	INFORMATION REQUIRED	DISPLAY OPTICYS
A/C PERFORMANCE	MONITOR & CONTROL PITCH & BOLL POYITOR & CONTROL VAM MOMITOR & CONTROL ALTITUDE MONITOR & CONTROL ALTITUDE RATE MONITOR & CONTROL HEADING MONITOR & CONTROL HEADING MONITOR & CONTROL ANGLE OF ATTACK MONITOR & CONTROL A/C STATUS (FUEL, ENGLESH MONIT, ENGINES, ETC.)	MONITOR, ASSESS & RECORD	ANGLE AND RATE ANGLE AND RATE TERRAIN CLEARANCE AND PPES, ALT, ANGLE AND RATE ANGLE AND RATE RATE-TAS, MACH ANGLE MODE SELECTED PROPULSION FARAMETERS FUEL FLOM, ENSINE CONTROL	ADI, EADI, HDO ING. 1/51, V5D ALTIMETER, VENT BAR, S OF GREY VVI, V5D, VERTICAL BAR HDO, IND., HCD, A'N CHAR, T/51 ASI, VERTICAL BAR, A/N CHAR DISTTAL (A/H), MOVING MAP (DISCPETE) SYEBOL, A'N CHAR BAR SRAPH
NAVISATION 1 NAVATES 1 NAVATES 2 TERMIKAL NAV.	SELECT MAY, ALD EQUIFMENT (E.S., TACAN) SELECT OPER, MODE & FREGUENCY SELECT OTHER EQUIP, USING DISTANCE/ BEARING INFO, INCERT IP CORDINATES (SELECT & ENTER) INSERT PROFILE INSERT PROFILE INSERT RP CORDINATES INCERT BALLISTIC WIND MOULTOR, CONTROL & TRACK ESCAPE WPNS PROF MCULTOR, CONTROL & TRACK ESCAPE WPNS PROF MCULTOR, CONTROL & TRACK EVADE DEFENSES FRUFILE MCULTOR COMPUTED TIME INTERVALS	OBSERVE SELECTION/PERFORMANCE OBSERVE SELECTION/PERFORMANCE OBSERVE SELECTION/PERFORMANCE MONITOR INSERTION PROCESSES MONITOR INSERTION PROCESSES MONITOR STATUS MONITOR STATUS MONITOR STATUS MONITOR STATUS	EQUIP, SELECTED M/F SELECTED ILLUM IND., A TONE IND., EQUIP, SELECTED ILLUM IND., A TONE IND., ILAT/LONG A/N CHAR	ILLUM IND., A TORE IND., A'N C A'N CHAR A'N CHAR A'N CHAR A'R CHAR A'N CHAR
SEARCH & ACQUIRE	SELECT & ACTIVATE SENSOR JUSTIATE SEARCH (SELECT MODE /RANGE) ACQUISE TANGET SELECT VIGURE HASE SELECT VIGURE HASE VIEW AREA FOR DESCRIBED CUES	OSSERVE SELECTION/APPROPRIATENESS GENSOR SELECTED MCMITOR MCMITCR ACQUISITION MCMITCR ACQUISITION MCMITCR MCMITCR MCMITCR MCMITCR MOMITCR MOMI	SCHOOL SELECTED & ACTIVATED RATES SELECTED LOCATION (VISUAL) AID SELECTED ANGLE SPECIFIC CUES	11LUM 1ND., A TONE 1ND., A/N 1 11LUM 1ND., A TONE 1ND., A/N 1 11LUM 1ND., A TONE 1ND., A/N 1 11LUM 1ND., A TONE 1ND., J/N 1 A/N CHAR HOTTHS MAP

Table G-1 (Continued)

FUNCTION	PILOT TASKS	INSTRUCTOR TASKS	INFORMATION REDUINED	DISPLAY CPTICAS
133 PREPARATION	SELECT MEADON SELECT MEADON SELECT DELIVERY MODE SELECT DELIVERY RATE ARM MEADON SELECT/FRIFY SENSOR ALIGN COURSE WITH PREDICATED TANGET MOVITOR AT NATIONER LIMITS & ESTATIONS TRAY NAY, CRAY, MOVITOR ATC PROPERMY, CRAY, MOVITOR ATC PROPERMY, CRAY, PERIFY TRASET LOCATION RE KNOWN CHAR DESIGNATE TRAGET SELECT LOCY ON TO TARGET 1DEWITOR TRAGET LOCATION TO OTHER SYS NAVIGATE TO SPECIFIC COORDINATES	HOWITOR	MEADON SELECTED HODE SELECTED AATE SCIECTED WEAPON ANIED SENDON SELECTED LOCATION, FLIGHT PARAMETERS FILGHT PANAMETERS FILCH PANAMETERS FILCH PANAMETERS LAT/LONG LOCATION (VISUAL) OR , TIME MODE SELECTED LOCATION (VISUAL) SYSTEMS INTOWED FLIGHT PAPAMETERS	A/N CHAR, I LLUMINATED IND A/N CHAR, I LLUMINATED IND A/N CHAR, I LLUMINATED IND A/N CHAR, I LLUMINATES IND A/N CHAR, I LLUMINATES IND A/N CHAR, A/N CHAR, GPAPHIC W/CURSOR A/N CHAR, GPAPHIC W/CURSOR A/N CHAR, GRAPHIC W/CURSOR A/N CHAR, A/
MEAPON DELIVERY	CHECK WEAPON AVAILABILITY RAVICATE TO RP RELEASE WEAPON MONITOR WEAPONS EFFECTS FLY ESCAPE MANEUVERS FLY EVASIVE MANEUVERS	MONITOR MONITOR PROFILE MONITOR TIME MONITOR PROFILE MONITOR	AVAILABILITY CHICKED FLIGHT PROFILE PARAMETERS TIMING EFECTIVENESS MET FLIGHT PROFILE PARAMETERS FLIGHT PROFILE PARAMETERS	AUDIO INDICATOR HOVINS MAP, GRAPHIC A/N CHAR, AUDIO INDICATOR MOVINS MAPS, GRAPHIC MOVINS MAP, GRAPHIC

in Table 6-2.

For the IP to perform his auties efficiently he must possess a variety of inherent knowledges in addition to the specific skills. The IP must know now the simulator reacts to control inputs and what its limitations are. He must also know the operational role of the simulated system, its missions and intended use. Knowledge of simulator operation is obviously required. The training philosophy underlying the content and order of items in the training syllabus as well as the manner in which it must be followed should also be known and understood by the instructor pilot. The monitoring of stadent performance at the instructor's console for the purpose of evaluation requires considerations based on this philosophy.

Knowledge of the student pilotis relevant background of experience is also required as it may impinge on the approach to be used in training. To train a pilot to fly a jet-powered airplane when his prior experience was limited to propeller-driven machines would involve a considerably different process than training someone whose flying experience included an airplane which was closely similar to the one he is learning to fly.

The job knowledge required of the 1P, as well as specific activities involved, depends on the mission and operational characteristics. 1P job knowledge required to perform flight simulation training duty is shown in Table G-3.

Table G-2. Instructor Pilot Tasks, Processes, and Skills

Task	Process	<u>Skill</u>
Search for & receiving information	Perceptual	Detect, inspect, observe and scan
Identify objects or events		Discriminate, identify, locate
Process information	Mediacional	Categorize, calculate, code, compute
Problem solving/de- cision making		Analyze, choose
Communicating	Vocal	Advise, answer, direct, inform
Simple/discrete	Motor	Activate, connect, join, set
Complex/continuous	`	Adjust, align, regulate, synchronize

BYCKERONND SINDENI.S			×		×
TMTERFACE MAWACHINE			×	;	×
TACTICS YTIRALIRMAT	>	< ×	×	;	×
nnDeMENT PSYCHOLOGICAL		×	×		
TRAINING TECHNIQUES		×	×		
SIMULATOR CPERATIONS	× >	<	× ×	× :	×
OPERATIONAL ROLE	>	< ×	×	× :	×
REQUIRED KNOWLEDGE IP FUNCTION	MONITOR SYSTEM STATUS MONITOR OPERAT-	TONIT OF STUDENT PERFORMANCE MONIT OR STRIET ATOR	EVALUATE STUDENT PETFORMANCE	EVALUATE SYSTEM PERFORMANCE EVALUATE MAN-	MACHINE

Information Requirements

During the analysis of the IP's role and duties, we concluded that his job in simulator training can be generally categorized into five major functions: (1) simulator set-up, (2) problem set-up, (3) simulator/student performance monitoring and assessment, (4) communications, and (5) on-line/off-line decriefing.

Although IOS displays could be used in the performance of all of these functions, the third function, monitoring and assessment of performance, appeared to be the appropriate focus for this study. In reviewing the IP's monitoring duties, four general categories were identifier—(1) monitor only (results in no specific action), (2) monitor-record (results in IP recording information), (3) monitor-gecide—act (results in a decision which forces some kind of action) and (4) monitor—analyze (results in on—line assessment of system/student performance.

Information type and manner of display required by an IP depends on the operational situation. The relationship between the aforementioned categories of monitoring duty and mission segments selected is shown in Table G-4. Display information required by the IP was derived based on detailed task analysis of both the student and the IP, the results of which were presented earlier in Table G-1.

.ສ ເມ	DISPLAYED INFOAM ATION ADEQUACY	××	××	××	×××	× ×
VITOR	STUDENT PERTORM	×	××	××	×××	×××
MON ANA	QUALITY OF SYST PERFORMANCE	××	×	×	××	***
os in	OB COMINAGORS WISSION VEOBL	×	><	××	×××	
MONITOR DECIDE	MALFURCTION ISOLATION	×	×		×	× ×
M M	DISPLAY DISCRETE SUOUMITHUOUS	××	××	××	××	× ×
CCAD	SIMULATOR OP. INADECUACIES	×	××	.× ×	××	× ×
& 고	STUDENT PERFORMANCE	×	××	××	\times \times	×××
VITCR	OP, SEQUFNCE DIVIATION	×	××	×		×
NCW	SUTATS MATSYS	××	><	×	>< ><	× × ×
>-	SIMULATOR OPERATIONS	××	××	××	××	× ×
R ONL	STUDENT PERFORMANCE	×	>< ><	××	×××	×××
MONITO	DEERATIONAL OPERATIONAL		× ×	×		×
X.	TMSTRUMENT SUTATS	××	×		××	×××
3Zλ	JANA GWA ROTINOM	×	×	×		×
DE	WOWITOR AND DECI	× ×	><	××	×××	××
ВО	MONITOR AND RECO	××	××	×	×××	×××
	MONITOR ONLY	××	× ×	××	×××	× >< ×
TACTORICTOR	STUDENT TASKS FUNCTION CATEGORIES	A/C PEPFORMANCE FLIGHT PROFILE A/C STATUS	NAVIGATION HAV. AID SELECTION TERMINAL NAV.	SEARCH & ACQUIRE TOT. AREA LOCAL. VISUAL IDENT.	COMBAT PREPARATION TOT/WEAPON MATCH TOT/AC ALIGNMENT TST LOCK-GN	WEAPON DELIVERY RP HAVIGATION NEAPON RELEASE ESCALE MAYICATION

IV. BENCHMARK TASK

Benchmark Task Criteria

To be a suitable benchmark task, the task must be one which can be used to evaluate the effectiveness of different displays in meeting a wide variety of 1P information requirements. Accordingly, criteria for the development of the benchmark task must include: (1) criticality, (2) frequency, (3) complexity, (4) measurability, (5) implementability to multi-cockpit monitoring. These criteria are explained in the following discussion.

information that is pasid to the success of the IP performing his function. Since much of this information will vary from maneuver to maneuver, the benchmark task should contain information elements that are both critical and common across a large number of maneuvers. For example, the requirement for airspeed information is critical to many maneuvers and is controlled solely by actions of the student. On the other hand, while fuel pressure information would be critical to the student in the event of a fuel pump failure, this failure would have been instigated by the instructor, and therefore, the information would not be critical to the instructor.

Frequency. The benchmark task should contain subtasks which are

frequently performed by the IP. As used here, frequency includes both the amount of time spent performing a function and the number of times the function is performed. As with the criterion of criticality, for a function to satisfy the criterion of frequency, it should be considered frequent across a significant number of flight maneuvers. For example, the turn and bank indicator is monitored with high frequency during particular maneuvers but is seldom monitored at other times. Monitoring of altitude, however, is virtually continuous during all phases of flight and would unquestionably meet the frequency criterion.

Complexity. The IP job is complex. He must observe and integrate data to determine if the aircraft is at the desired point in space, at the desired speed or aceleration, and whether or not the aircraft is properly configured (power, trim, etc.) to produce the desired performance. For the Denormark task to be valid, it must require the IP to perform such complex functions.

Measurability. For the benchmark task to meet the criterion of measurability, it must lend itself to the taking of quantitative measures. This will help ensure that the display evaluation is objective rather than subjective. That is, the derived figure of merit for a given display must be based on now effectively or efficiently the information required by the IP has been displayed as opposed to how well the IP liked the display.

Implementability. As used nerein, the criterion of implementability refers to the ease with which the benchmark task can be used in a laboratory setting for the evaluation of alternative displays. This requires that the source data for the generation of information to be displayed be in a format which, if not common to, is at least easily adaptable to present and anticipated display hardware.

Multi-Cockpit Monitoring. The establishment of a benchmark task suitable for use in the evaluation of displays to be used for multi-cockpit monitoring requires that the information presented be taken from maneuvers considered reasonable candidates for multi-cockpit instruction.

Benchmark Task Development

A review of the IP Job Analysis reported in Section III of this appendix reveals that the IP's prime function is to monitor. Furthermore, information relative to basic aircraft flight parameters is required during all phases of flight regardless of the procedure or maneuver being flown. While a wide variety of maneuvers of varying length and complexity could be used to generate the information which would satisfy the benchmark task criteria, five basic flight maneuvers, climb and level-off, descent and level-off, level turn, climbing turn, and descending turn were selected on the basis of their

comprehensiveness, representativeness, and simplicity. Analysis of these maneuvers reveals that the transition and steady-state conditions could be strung together in a manner which would describe almost any flight maneuver. While this concept may have certain limits, the maneuvers selected are considered to generate the majority of 12 information requirements relative to the monitoring of aircraft control performance. The 1P information requirements generated by these maneguers are representative of those found in most flight training situations and satisfy the criticality, frequency, and complexity criteria. The parameters used to define these maneuvers lend themselves to the collection of quantitative data as required by the measurability criterion. In view of the fact that the maneuvers are not very complex and can be adequately displayed through indications of five flight parameters, i.e., airspeed, attitude, altitude, vertical velocity, and heading, there should be very little problem developing source data to implement the benchmark task on a wide variety of displays. Furthermore, the maneuvers and the task of monitoring flight instruments are typical of what is expected to be encountered in a multicockpit monitoring situation.

In summary, the benchmark task developed for this effort consists of monitoring five flight parameters (airspeed, attitude, altitude, vertical velocity, and heading) during ten flight segments consisting of two repetitions of five basic flight maneuvers (climb and level-off, descent and level-off, level turn, climbing turn and descending turn). The

manner in which the flight segments were developed and presented and the manner in which the benchmark task was performed and tested are covered in detail in Section VI of this Appendix.

V. PERFORMANCE MEASURES

The objective of this phase of the effort was to develop performance measures which would discriminate the relative effectiveness of alternative display formats and configurations. Display effectiveness is best defined as the ability of a display to impart desired information to an observer. In that there are no means to directly measure this ability, it was necessary to devise some means of determining now much displayed data had in fact peen perceived by the observer. Since the IP cannot respond to something he has failed to notice, the most straightforward way to measure display effectiveness is to getermine whether the information on the display was noted by the IP and, if so, now much of it was retained. Accordingly, the procedure developed to do this required subjects to observe displayed flight information generated oy a series of short simulated flight seuments and to respond to questions concerning the values of certain of the displayed flight parameters at specific points during the segment. This approach is desirable in that a response may be obtained regardless of the quality of flight or the observer's knowledge of such things as correct procedures or aircraft performance characteristics. The observer is not required to judge the goodness of what he has observed but merely to report that which has been observed.

On the basis of the 1P information requirements determined during the IP task analysis (see Table G-2), we developed eight questions for each of the five basic maneuvers. The manner in which these questions were employed to collect data is discussed in detail in Section VI.

There was no clear way of establishing what limits should be set for scoring a response as "correct"; therefore, we examined the collected data and selected limits which would provide maximum sensitivity to the effects of various conditions. Since this was not an evaluation of displays but rather a search for a feasible means to evaluate such displays, this was considered to be both a proper and necessary manner in which to proceed.

In scoring responses to the questions on altitude or vertical velocity, a response in error greater than 500 feet was considered incorrect and scored zero, an error of less than 500 feet was considered correct and scored one. The choice of 500 feet as a cut off point was based on a first cut analysis of the raw data which indicated that 500 foot cut off point would provide a measure with good sensitivity to variability of performance. Similar rationale led to establish a five degree error limit for heading, roll, and pitch and a corresponding ten knot allowable margin for airspeed.

In the absence of sufficient data to establish statistically reliable response distributions, no attempt was made to give differential credit for more accurate responses.

In summary, the metric of display effectiveness used was an indirect measure based on the percentage of correct observer responses made to questions about displayed flight information, where the criteria for "correctness" were estimated by the investigators.

VI. DEMONSTRATION AND TEST PROCEDURE

Approach

As stated previously, the objective of this research was to develop a means of evaluating the relative effectiveness of candidate flight simulator instructor/operator station displays. The approach taken was to develop a benchmark task and performance measure such that when the benchmark task was performed using alternative displays and the performance measures applied, relative effectiveness of the displays could be determined. Toward this end, the benchmark task established was one which required an observer to view prerecorded flight information on a candidate display and to respond to questions about the displayed information.

General Discussion. To demonstrate the above approach and to test its feasibility, four test observers performed the benchmark task using both an analog flight instrument display and a CRT digital display. The test conducted was a first look at the feasibility of the benchmark task approach and as such did not produce sufficient data for rigorous statistical analysis. However, it was considered to be a reasonable compromise between a vigorously quantitative test and a purely subjective one.

Test Subjects. Four test subjects were used for this test. Inree of the subjects were well qualified pilots with prior military flying, over 3,000 pilot hours, and experience as instructor pilots. Qualification of the fourth subject was limited to flying experience of about 40 nours of piloting a light plane under visual flight rules (VFR) conditions only. The rationale for including a subject with minimum experience was to gain some initial data on whether or not extensive prior experience using a standard instrument display might inhibit the experienced pilot's ability to work with a non-standard display format, viz., the CRT digital display, or otherwise bias the data in favor of the standard display. Presumably, the nighly experienced pilot would have a relatively greater difficulty with the strange format than someone who was not overpracticed with the standard instrument display. The preliminary test thus represented a broad range of experience, and individual differences in apility on the task were accentuated by this selection.

Test Material. The displays representing the five maneuvers previously discussed constituted the test materials of the denomnark task. The two types of displays used were standard flight instruments and digital presentations on the CRT. The instrument panel had the display indicator, the attitude indicator (artificial norizon), the vertical velocity indicator, heading indicator, and the altimeter. The arrangement of flight indications on the CRT was identical to the instrument panel. No other instruments in the instrument panel were activated. On the CRT, all of the indications were presented in digital form, white on black dackground. For pitch and roll information, the symbols "UP," "DN," "L," and "K" appeared to the left of the digits as appropriate.

The CRT was located just above the instrument panel at the same viewing distance as the analog instruments. The information was displayed simultaneously on the instruments and CRT. The CRT unit had a cover which could be positioned over the tube face when the information was to be viewed on the instruments. Instruments were likewise covered when the CRT was exposed.

Test Facility. The experiment utilized a general purpose simulation facility, multi-mission simulator (MMS) developed for conducting research requiring man-in-the-loop simulation.

Figure 6-2 is a block diagram showing the major elements of the

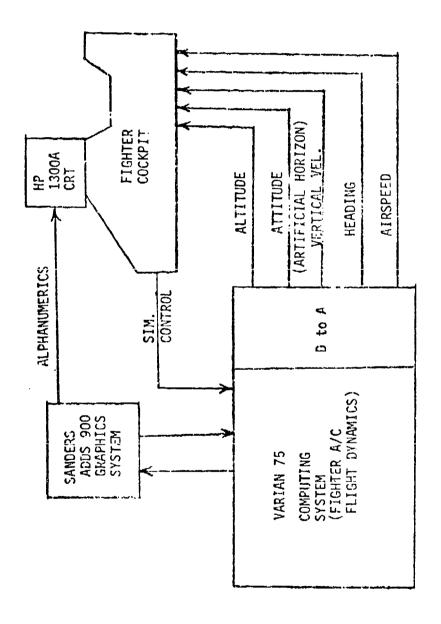


Figure G-2. Major Elements of Flight Simulator

flight simulator utilized. "CANNEO" missions were provided by flying closed-loop man-in-the-loop mission segments and recurring the pilot input commands to the aigital computer.

The Varian 75 computing system solves the equations of motion of a representative fighter aircraft and provides simultaneous display inputs to a Sanders Adus 900 graphics system and to the flight instruments in the simulated fighter cab.

The Sanders graphics system provides digital information for display on a 10-inch Hewlett-Packard 1200A CRT. The digital information displayed on the uRT represents the same type of information provided to the analog flight instruments (altitude, attitude, and heading). Simultaneous information was provided to both the uRT and the flight instruments. Special masks were used over the displays which allowed the test subject to view either the analog flight instruments or the digital display on the CRT.

Only the rear station of a two station cockpit was utilized, and the Hewlett-Packard CRT was mounted directly above the rear station flight instrument panel. The arrangement of the analog flight instruments was as shown in Figure G-3.

Existing software was used which had been developed for an Advanced Tactical Fighter Simulation. This program was made up of standard modules and aircraft-unique modules. There were six standard modules

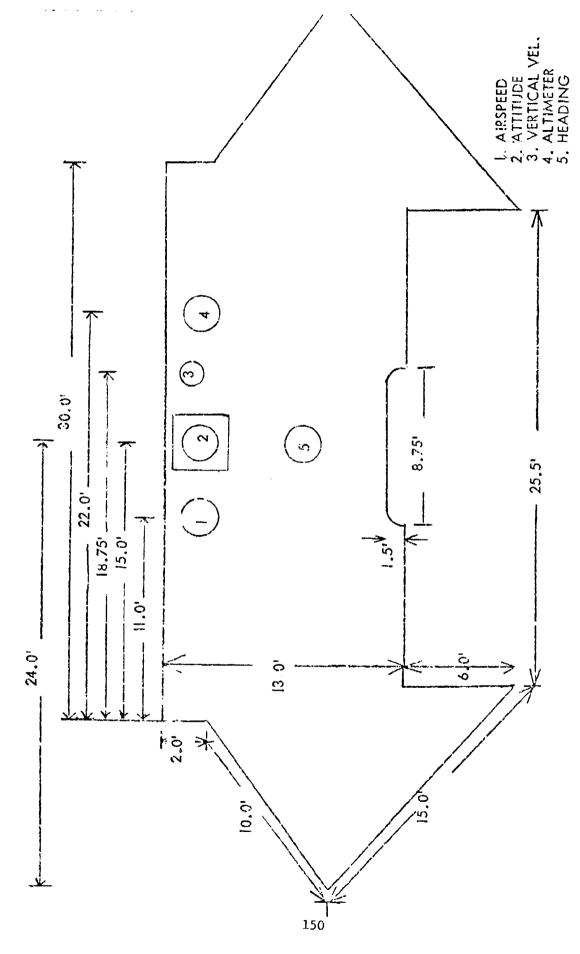


Figure G-3. Arrangement of Analog Instruments in Crew Station

used in this simulation. Four of those (transformation matrix, equations of motion, integration, and aircraft related quantities) provided the capability to determine the aircraft trajectory, orientation, and dynamic response. The remaining two standard modules (atmosphere and winds) provided the natural environment surrounding the aircraft. The equipment used included two Varian 75 minicomputers with 48K lo-bit words of memory each. One computer was used to drive the graphics, and the second was used to simulate the fighter.

Test Procedure. The five maneuvers were flown four times each two duplicates of each maneuver on each of the two display formats, for a total of twenty flight segments. Prior to presenting these to the test subjects, the flight segments were randomized. Eight questions were generated (Appendix I) for each of the five maneuvers and these were also randomized. The randomized displays, questions, and flight segments are shown in Appendix J. A randomized set of four questions was given after the first replication of a given maneuver shown on a display, and the remaining four were given after the second replication of the same maneuver shown on the same display. Specific test procedures for each of the subjects were as follows:

The subject was seated in the cockpit of the MMS with the experimenter sitting beside him outside the cockpit. He was given written briefing material to read consisting of general instructions τ_0 , the effect that all the participant was required to do was to doserve indications as directed on either the analog instruments or on the CkT.

After the subject finished reading the oriefing instructions, he was shown now to position a special mask to occlude the indications on the display which he was not to use, and how to expose those he was to use. (During the test, the experimenter ensured that the proper display was indeed occluded.) The observer was then given a typed set of instructions regarding his task (Appendix D). These were intended to prepare him for the kinds of questions he would be asked. The subject was then presented with a randomized flight segment on one of the two displays for a duration of 1-2 minutes (depending on the particular flight segment). At the conclusion of the presentation, he was asked four pre-randomized questions by the experimenter. This procedure was repeated for each of the 2D flight segments, with a five-minute dreak after 1D flight segments. The session for each subject was completed in approximately one and a half hours including the break. The subjects had no practice on either of the test displays prior to the actual testing.

After all four subjects had completed the experiment, they were debriefed in an informal, unstructured manner. The results of this debriefing are treated in Section VII. (Results and Discussions).

VII. RESULTS AND DISCUSSION

The test conducted was concerned primarily with demonstrating the feasibility of the benchmark task approach for the evaluation of displays to be used at a remote IUS. Since insufficient data were taken to

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perform statistical tests of differences, the only "analysis" performed on the data was the summing of correct responses across the several factors.

Overall performance (all subjects and all flight segments) was derived by summing all the correct responses by four subjects to the questions about the twenty flight segments viewed on two displays, and dividing that sum by the total number of questions asked. The resultant outcome of this calculation of 66% was a fortunate one in that it is in a range which allows for variability in both directions. Unviously, a mean percentage of control responses close to zero or one number would have forced the distribution to be skewed and would have indicated that the questions were either too difficult or too easy.

The major factor in the test was display type. We expected that the standard instruments would prove more efficient for use by those already familiar with this type of display than the all-digital display on the CRT. The results support this expectation in direction but not in magnitude of the difference, 60% correct for instruments and 64% for CRT. This small difference would not likely be statistically significant, considering the relatively large variability due to other factors. It should be noted, nowever, that had the method of scoring been more sensitive, e.g., differential rather than binary, the magnitude of the difference might be more substantial.

As shown in Table G-5, the range in scores (80% to 55%) due to pilct

Table G-5. Data Sammary by Display, Maneuver, and Pilot

		No. of Correct Responses										
	·		Iı	ıs tru	ment			CR'F				
Pilots	P.	В	Ç	Ð	Σ:	0/ /3	А	В	С	D	Σ	%
Maneuver				-					•			
Climb	8	4	7	8	26	81	6	5	6	7	24	75
Level Turn	7	3	6	4	20	62	5	4	7	7	23	72
Descent	5	5	7	6	23	72	7	4	6	7	24	75
Climbing Turn	3	4	6	3	16	50	4	3	4	3	14	44
Descending Turn	6	6	6	5	23	72	6	2	4	6	18	56
Σ	29	22	32	26	108	· .	28	18		30	103	
0/ /o	72	55	08	65	68		70	45	<u>0</u> 8	75	(4	

differences with instruments is 25 percentage points, while with the CKT, it is 30 percentage points 75% and 45%). This is six to seven times the range in scores due to display differences 66% and 64%. If we compare correct responses for individual subjects, we see that Pilot A distributed his correct responses nearly evenly between the two displays, Pilots B and C gave 55% and 54% of their correct responses, respectively, to instruments, and Pilot D gave only 46% of his correct responses to instruments. Pilots A, B, and D have many nours of experience looking at instruments while Pilot C has only a few and all of Pilot C's flying has been VFR. Thus, the experience factor does not seem to account for the differences among pilots in this study.

We might note further that less experienced Pilot C not only was the top performer with instruments but also showed the largest difference in favor of instruments. One might have thought this pilot would have performed relatively better with the CRT display than would the pilots with long experience using instruments. Pilot c also had the best performance overall, which also was a finding not producted. Although looking for "reasons" benind the observed differences almong subjects is merely speculative, one is tempted to suggest that the superior performance of Pilot C may be due to youth more than anything else. Profering an alternate potential explanation, it might be suggested that a lot of experience leads pilots to be more selective in their monitoring of flight indications.

Comparing display formats at the level of the individual maneuvers, we observe differences of an inconsistent nature. In two of the five

maneuvers, the total percent correct responses over all subjects is numerically higher for the dRT display. No inferences are urawn with regard to the confidence to be placed in such an observation (as with other observations in this discussion) but, on the other hand, it would weaken any tendency to take seriously the overall performance difference in favor of instruments.

As to the differences in correct responses for the various maneuvers, the data sorted in this way are very naru to interpret. The eight questions for each maneuver were not generated with a requirement that they be of equal difficulty among maneuvers. Not even the simplicity of the maneuver is reflected in any consistent way in the responses. Why should a climbing turn be more difficult to monitor than a descending turn? But then, we have no reason to assume equivalence in the conditions present in the test.

When the data are summarized by maneuver and flight indication (Appendix L), the numbers in individual cells are too small to discuss, but in a larger study, one may be able to place flight indications in order of importance and monitoring difficulty. Since the same flights were seen where instruments were monitored as when the indications were presented on the CRT, and, similarly, the same questions were asked, we may assume that where differences between the two displays are large, there is a strong suggestion that the observed difference would not up in a larger study. For example, questions about altitude were answered correctly 70% of the time when the information was read from the

instruments out only 50% of the time from the CRT. Roll also was read more often correctly (and remembered) with the instruments, 90% as opposed to 60% of the CRT. On the other hand, pitch questions were scored correct only 56% of the time with instruments, but 81% with the CRT. The other three flight indications show much smaller differences between displays.

One would expect to see learning over the course of the twenty flight segments because of the unusual character of the task. As shown in Appendix M, two of the pilots (B and C) show some evidence of learning based on the number of correct responses in each quarter of the questions. However, pilots A and D shown no learning trends.

After all pilot observers had completed their participation in the test, they were given an opportunity to express their opinion adout the techniques used. They indicated that the task was a difficult one, primarily because they did not know what the maneuver was to be or what questions they would be asked. They pointed out that in flying to an artificial norizon they are less interested in the specific values if the airplane is in the attitude they intend it to be in, whereas the CRT display required them to read the digital presentation. The least experienced pilot missed the "seat of the pants" feedback experienced in a light airplane.

when asked about the task of an instructor pilot as represented in the development of better displays for an luS, they pointed out the individualistic approach to the use of instrument indications, suggesting that one arrangement might not pest suit all IPs. They also felt that the interaction between IP and student must be tailored to the situation and the personalities of both. Should the IP be simply a checker of student activity? Should be adopt a tutorial attitude? Should be behave like a martinet? Should be concentrate on building the student's confidence? No single answer can be given.

VIII. CONCLUSIONS AND RECOMMENDATIONS

While the scope of this program did not permit quantitative scaling of responses, it did allow for quantitative comparison amony displays. Although the evidence is not unequivocal, the test conducted demonstrated that the approach used is feasible for the evaluation of displays and could prove useful in the development of design specifications for displays to be used at a remote 105.

If more data could be collected and the questions and responses refined, the development of an "instructor pilot standard observer" representing average monitoring abilities and tendencies would be possible. With the collection of sufficient data, standardized scores could be computed which would permit future evaluations to be made against a scale having the necessary statistical properties.

A problem associated with the approach used is that the IP quite often looks at the flight indications as a group rather than a set of individual indications. That is, if the combination of indications in a

given instance is correct, the 1P may not take particular note of each specific value, but merely satisfy nimself that indications are correct in aggregate. Should this occur, although the display performed its function of providing the information, the observer may not be able to respond to a question relative to its value at that point in the maneuver. However, careful analysis, to ensure that the questions asked pertain to information considered important at a certain point in the maneuver, should minimize this problem.

while every effort was made to develop a benchmark task applicable to the product possible range of 12 monitoring functions, the scope of this effort did not permit development of maneuver segments which would generate all of the 12 information requirements. Additional work is required to determine what all of the 12 information requirements are.

The present study has shown that one should expect a wide variation in the ability to monitor instruments, or other displays, even for highly experienced pilots. This may mean that IPs, if more carefully selected and/or trained, could show greater efficiency in their monitoring performance.

The penchmark task approach quite obviously should undergo considerable refinement before its utility can be validated. Extension of the present effort should include thorough study of the training situations of interest. Perhaps more important, future studies need to explore the use of more sensitive measures of performance on the benchmark task. Instructor tasks and the information needed to perform

them should be researched more thoroughly. Meaningful alternative approaches to display techniques could then be compared for effectiveness and cost.

While this effort was directed towards developing a means of evaluating rather than of designing displays, the work evoked considerable thought and discussion relative to design. This information is summarized in the following paragraphs.

An effort should be conducted relative to optimizing the display format according to the type of information. Pointers and dials may remain pest for certain indications out most likely not for all the indications they are used for the typical cockpit. Good inspection of trends, for example would certainly be easier with a display that showed more than the present status, e.g., a simple graph of flight status vs. time.

The type and format of information presentation is a significant factor. For example, an altitude profile displayed on a GRT may permit an IP to keep track of a student with less effort. On the other hand, a single digital indication may be sufficient for the recording of extreme values for something like maximum 6 force or exhaust gas team rature.

Another way to enhance the capacity of a display and the speed of response or retention of details by the LP is the use of a color UKI. Color may be used to separate types of indications more clearly or it may

or used to show the severity of a condition, e.g., red for low fuel reserves or angles of attack close to stall conditions.

The constraints of the cockpit environment should not be retained for the IOS if some other display technique will permit the IP to perform his task more easily. If the IP does not have to monitor all instruments, he shouldn't have them cluttering up the IOS display area. Furthermore, if the display format enhances those indications requiring his attention, the IP may be able to monitor several students at the same time.

A program of research in IUS displays from the standpoint of human resources should include a strong emphasis in visual perceptual abilities. Differential sensitivity associated with retinal location are particularly important in a monitoring task since the relatively low acuity in the periphery means that some way is needed to bring the observer to fixate the indication of importance with central high acuity vision. (A flashing light has been successfully used for this.)

In summary, the benchmark task approach to 105 display evaluation is considered feasible and further refinement and investigation is recommended.

BIBLIUGKAPHY FUK APPLINDIX G

- Alba, E. A time-based methodology for assessment of individualized performance. Washington, U.C.: U.S. HEW, April 1972.
- **Arntz, N.J. Methodology for the definition of a space vehicle display system. Technical Paper Published in the Society for information display, 1971.
 - demenati, A.T., Hull, R., Korobow, N., & Mieualtowski, W. <u>Development of an automatic monitoring system for flight simulators.</u>

 AMKL-TDR-62-47, AD-283 OD8. wright-Patterson Arb, UH: May 1962.
- **Blaiwes, A.S., et. al. Transfer of training and measurement of training effectiveness. Human factors, 1970, 14(6).
 - Bradley, A. Experimental design for quantitative measurement and evaluation of pilot performance on cockpit displays. NADC, (AD-833-432L) June 1961.
- *Brecke, F., & Reiser, R. <u>Critical components of flight instruction</u>
 as perceived by Instructional Resources Laboratory, November 1972.
- *Brooker, S.E. Instructor console instrument simulation. (AU-751-759). HTtc, September 1971.
- Caro, P.W. Aircraft simulators and pilot training. (AU-AUUZ-ol4). Alexandria, VA: Human Resources Research Urganization, 1973.
- control. Hum RRO Professional Paper II-12, July 1972.
- **Connelly, E.M., Bourne, F.J., Loental, D.G., & Knoop, P.A.

 Computer-aided techniques for providing operator performance

 measures. AFHRL-TR-74-87. AD-AD14 330. wright-Patterson Ard, OH:

 Advanced Systems division, Air Force Human Resources Laboratory,

 December 1374.
- **Connelly, E.M., Schuler, A.P., & Khoup, P.A. Study of adaptive mathematical models for deriving automated pilot performance measurement techniques: Model development. AFHKL-TK-09-7(1).

 AD-704-597. wright-Patterson AFB, OH: Training Research Division, Air Force Human Resources Laboratory, October 1969.
 - Cyrus, M.L., & Woodruff, R.R. <u>Grading system for T-4G simulator students</u> in <u>UPT studies</u>. AFHRL-TR-74-91. AD-A004 605. Williams AFB, AZ: Flying Training Division, Air Force Human Resources Laboratory, November 1974.

^{*} and ** Reports identified as most applicable and reviewed in detail.

** Reports reviewed in greatest detail.

APPENDIX H: LITERATURE SURVEY ABSTRACTS

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ABSTRACTS OF RELEVANT LITERATURE, Sheet 2 of 4

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APPENDIX I: TEST QUESTIONS

CLIMB AND LEVEL OFF

Cl	At what altitude did the aircraft start to nose over to level flight?
C-2	What was the highest altitude reached?
C-3	At level off, what was the heading?
C-4	What was the vertical velocity just before the start of level off?
C-5	What was the highest airspeed in the climb?
C-6	What was the roll angle in the transition from climb to level flight?
C-7	What was the maximum pitch up angle?
C-8	What heading changes were there, if any?

Correct Anguers

	Flig	ght Segmen	t Number		
Question	1	2	3	4	Unit
C-1	19670	19880	19500	19700	ſt.
C 2	1 9830	20010	19940	19920	ft.
C- 3	0	O	O	1	degrees
C- 4	5 8 0 0	58 0 0	5800	3100	ft/min.
C-5	360	680	3 65	350	knots
C ₇ 6	0	0	0	}	degrees
C-7	23	29	15	12	degrees
C-8	0	Ú	0	0	degrees

LEVEL TURN

LT-9	What was the maximum roll angle?
LT-10	What was the minimum altitude during the turn?
LT-11	What was the maximum altitude during the turn?
LT-12	At what heading did the roll out begin?
LT-13	What was the airspeed just before roll-in?
LT-14	What was the airspeed just after roll out?
LT-15	What was the maximum airspeed in the turn?
11-16	What was the minimum airspeed in the turn?

Correct Travers

Flight Segment Number							
Question	5	6	7	8	Unit		
LT-9	34	32	2 8	33	degrees		
LT-10	19810	20030	19710	1 9690	ft.		
LT-11	20400	20950	20100	20580	ft.		
LT-12	131	176	92	263	degrees		
LT-13	280	255	270	275	knots		
LT-14	275	245	270	265	knots		
LT-15	280	260	295	290	knots		
LT-16	275	235	265	270	knots		

DESCENT

D-17	What was the pitch angle when the mose was lowesc?
D-13	What was the airspeed just before the aircraft nosed over for the descent?
D-19	What was the airspeed just after level-off?
D-20	What was the altitude prior to the descent?
D-21	What was the altitude after the descent?
D-22	What was the initial heading?
D-23	What was the heading after level off?
D-24	What was the maximum roll angle (left or right)?

Correct Answers

	I	"light Segm	ent Number		
Question.	9	10	11	12	Unit
D-17	-1	- 7	- *3	- 6	degrees
D-18	310	285	29 5	290	knots
D-19	315	300	285	295	knots
11-20	20000	20220	20130	20240	ft.
0-21	15370	15100	15490	15170	ti.
D-22	0	0	0	0	degrees
D-23	0	0	2	0	degrees
D-24	0	0	2R	1 1R	dagnees

CLIMBING TURN

CT-25	What was the airspeed just after roll out?
CT-26	At what heading did the rol! out begin?
CT-27	At what heading did the roll out begin?
CT-28	What was the maximum pitch-up angle?
CT-29	What was the highest airspeed in the climb?
CT-30	What was the vertical velocity just before start of level off?
CT-31	At level off, what was the heading?
CT-32	At what altitude did the aircraft start to nose over to level flight?

Correct Answers

Question	13	Flight Segn 14	ment Number 15	16	Unit
CT-25	345	255	335	400	knots degrees degrees knots ft/min. degrees
CT-26	126	122	107	260	
CT-27	40	27	29	38	
CT-28	9	19	11	16	
CT-29	350	270	345	390	
CT-30	3050	4000	4300	4950	
CT-31	127	122	107	262	
CT-32	19750	19800	20140	20,40	

DESCENDING TURN

DT 33	At what heading did the roll out begin?
D7-34	What was the pitch angle when the nose was lowesi?
DT-35	What was the airspeed just before the aircraft nosed over for the descent?
DT-36	What was the airspeed just after level-off?
D1-37	What was the altitude prior to the descent?
DT-38	What was the altitude after the descent and level-off?
DT-39	What was the initial heading?
DT-40	What was the maximum roll angle (left or right)?

Correct Answers

Flight Segment Number									
Question	17	18	19	20	Unit				
DT-33	216	167	84	2 62	degrees				
DT-34	-]	~ 5	4	- 5	degrees				
DT-35	300	295	300	300	knots				
DT-36	295	300	350	315	knots				
DT37	20000	20320	19890	20000	ft.				
DT-38	15520	13360	15230	15810	ft.				
DT-39	0	0	0	0	degrees				
DT-40	39L	47R	32 R	32L	degrees				

APPENDIX J: TEST CONDITIONS AND DATA

	Pilot A									
	Mancuver	Flight Segment	Display	Question	Reported	Indicated				
1)	LT	8	CRT	10 16 11 15 rect = 1	?* 245 20,000 285	19,690 ft 270 kt 20,580 ft 290 kt				
2)	CT	14	CRT	29 28 30 25 rect = 2	225 14 4,000 225	270 kt 19° 4,000 ft/min 255 kt				
3)	DT	18	CRT Cor	37 36 38 33 rect = 3	20,000 300 15,000 165	20,320 ft 300 kt 13,360 ft 167°				
4)	СТ	13	inst. Cor	30 28 26 31 rect = 1	4,000 ?* 115 125	3,050 ft/min 9° 126° 127°				
5)	Lī	5	inst. Cor	14 12 10 15 rect = 3	280 ?* 19,900 280	275 kt 131° 19,810 ft 280 kt				
6)	D	9	inst. Cor	22 20 18 23 erect = 3	0 ?* 310 0	0° 20,000 ft 310 kt 0°				
7)	c	1	inst. Cor	6 4 2 7 rrect = 3	0 5,000 19,900 20	0° 5,000 ft/min 19,830 ft 23°				
8)	С	4	CRT Cor	2 8 3 7 rrect = 4	19,900 none 0 10	19,920 ft none 1° 12°				

^{*} Indicates the response "I don't know."

	<u>Maneuver</u>	Flight Segment	Display	Question	Reported	Indicated
9)	D	12	CRT	18 24 19 23 ect = 3	300 6 325 0	290 kt 11°R 295 kt 0°
10)	D	10	CRT	21 20 22 17 ect = 4	15,000 20,000 0 -7	15,100 ft 20,220 ft 0° -7°
11)	D	11	inst.	24 19 21 17 ect = 2	3 300 15,500 ?*	2° 285 kt 15,490 ft -7°
12)	TO	20	CRT	34 40 35 39 ect = 3	-2 25 300 0	-5° 32° 300 kt 0°
13)	DT	19	inst.	40 35 37 33 eect = 3	29 300 20,000 ?*	32° 300 kt 19,890 ft 84°
14)	CT	15	inst.	32 27 29 25 ect = 2	19,500 25 360 340	20,140 ft 29° 345 kt 335 kt
15)	LT	7	inst. Corr	16 11 13 9 rect = 4	270 20,250 280 28-30	265 kt 20,100 ft 270 kt 28°
16)	С	2	CRT	5 4 6 1 rect = 2	615 5,800 0 ?*	680 kt 5,800 ft/min O° 19,880 ft

^{*} Indicates the response "I don't know."

	Maneuver	Flight Segment	Display	Question	Reported	Indicated
17)	ст	16	CRT	26 32 27 31 rect = 2	?* 19,800 33 260	260° 20,740 ft 38° 262°
18)	DT	17	inst.	38 36 34 39 rect = 3	15,500 300 ?* 0	15,520 ft 295 kt -1° 0°
19)	С	3	inst. Cor	8 3 1 5 rect = 4	+4 4 19,500 370	none 0° 19,600 ft 365 kt
20)	LT	6	CRT Cor	13 12 14 9 rect = 4	245 176 250 29	255 kt. 176° 245 kt 32°

Pilot B

	Maneuver	Flight Segment	Display	Question	Reported	Indicated
1)	D (11	CRT Corr	22. 23 18 24 Pect = 3	0 4 390 4	0° 2° 295 kt 2°
2)	LT	6	inst. Corr	13 14 15 10 rect = 1	280 280 280 20,300	255 kt 245 kt 260 kt 20,030 ft
3)	LT	7	CRT	14 15 10 16 Pect = 4	270 295 19,500 270	270 kt 295 kt 19,710 ft 265 kt
4)	DT	19	CRT	33 39 34 40 rect = 0	19,300 ?* -15 25	15,230 ft 0° -4° 32°
5)	D	9	CRT	19 21 17 20 rect = 1	340 19,300 -1 24,000	315 kt 15,370 ft -1° 20,000 ft
6)	DT	17	CRT Corr	35 37 33 36 rect = 2	290 21,000 340 295	300 kt 20,000 ft 216° 295 kt
7)	C	2	inst.	5 6 7 2 rect = 1	700 0 10 19,300	680 kt 0° 29° 20,010 ft
3)	СТ	15	CRT	30 31 26 32 rect = 0	?* 100 80 18,000	4,390 ft/min 107° 107° 20,140 ft

^{*} Indicates the response "Idon't know."

	Maneuver	Flight Segment	<u>Display</u>	Question	Reported	Indicated
9)	D	10	inst. Corr	21 22 23 18 eect = 2	13,300 0 0 380	15,100 ft 0° 0° 285 kts
10)	TD	18	inst.	37 38 39 34 ect = 4	20,000 13,000 9 -5	20,320 ft 13,360 ft 0° -5°
11)	LT	8	inst.	16 11 12 9 ect = 2	300 20,300 300 31	270 kt 20,580 ft 263° 33°
12)	LT	5	CRT Corr	11 13 9 12 ect = 0	24,000 295 15 024	20,400 ft 280 kt 34° 131°
13)	ΰ	12	inst.	24 19 20 17 Pect = 3	10 320 20,400 -10	11° R 295 kt 20,240 ft -6°
14)	С	4	inst.	8 3 4 1 Pect = 3	none 0 4,000+ 19,300	none 1° 3,100 ft/min 19,700 ft
15)	СТ	13	CRT	27 29 25 28 rect = 3	44 345 330 10	40° 350 kt 345 kt 9°
16)	C	1	CRT Corr	3 5 1 4 rect = 1	0 345 13,000 200	0° 360 kt 19,670 ft 5,800 ft/min

	<u>Maneuver</u>	Flight Segment	<u>Display</u>	<u>Question</u>	Reported	Indicated
17)	СТ	14	inst. Corr	29 30 31 26 rect = 3	280 4,000 + 120 090	270 kt 4,000 ft/min 122° 1 22°
18)	PT	20	inst. Com	40 35 36 37 rec. = 2	30 280 300 260	32° L 300 kt 315 kt 262°
19)	c .	3	CRT	6 7 2 8 rect = 4	0 14 19,700 none	0° 15° 19,940 ft none
20)	СТ	16	inst. Cor	32 27 28 25 rect = 1	20,600 32 10 320	20,740 ft 38° 16° 400 kt

Pilot C

	Maneuver	Flight Segment	Display	Question	Reported	Indicated
1)	LT	6	CRT	14 15 16 10 rect = 4	240 260 240 20,000	245 kt 260 kt 235 kt 20,030 ft
2)	C	3	inst. Corn	6 3 1 2 rect = 4	0 0 20,000 20,000	0° 0° 19,600 ft 19,940 ft
3)	DT	17	inst.	36 40 39 37 rect = 4	300 35 0 20,000	295 ft 39° 0° 20,000 ft
4)	СТ	16	CRT Cort	28 27 25 29 rect = 2	16 26 390 330	16° 38° 400 : . 390 kt
5)	C	2	CRT Cort	6 7 8 2 rect = 3	0 15 1 19,990	0° 29° none 20,010 ft
6)	LT	7	inst.	14 11 9 10 rect = 3	300 20,000 25 19,600	270 kt 20,100 ft 28° 19,710 ft
7)	СТ	15	inst.	30 27 25 26 rect = 2	2,000 30 340 80	4,300 ft/min 29° 335 kt 107°
8)	DT	19	inst. Cor	38 35 33 34 rect = 2	16,000 300 80 Y	15,230 ft 300 kt 84° -4°

^{*} Indicates the response "I $\mbox{don}^{\, \rm t} t \ \mbox{know."}$

	Maneuver	Flight Segment	Display	Question	Reported	Indicated
9)	DT	20	CR: Corr	36 35 33 37 ect = 2	300 300 250 20,000	315 kt 300 kt 262° 20,000 ft
10)	D	11	inst. Corr	22 19 17 18 ect = 3	0 250 -10 300	0° 285 kt -7° 295 kt
11)	D	10	CRT	22 23 18 24 ect = 3	0 0 295 7	0° 0° 285 kt 0°
12)	D	12	CRT	19 20 17 21 ect = 3	350 20,000 -9 15,000	295 kt 20,240 ft -6° 15,170 ft
13)	С	4	CRT	4 3 1 5 ect = 3	2,000 1 20,000 350	3,100 ft/min 1° 19,700 ft 350 kt
14)	C	1	inst.	4 8 7 5 ect = 3	5,000 none 20 350	5,800 ft/min none 23° 360 kt
15)	Ū	9	inst.	20 24 23 21 ect = 4	20,000 0 0 15,500	20,000 ft 0° 15,370 ft
16)	LT	5	inst.	12 16 15 13 ect = 3	120 230 280 280	131° 275 kt 280 kt 280 kt

	Maneuver	Flight Segment	Display	Question	Reported	Indicated
17)	СТ	13	inst.	28 32 31 29 rect = 4	8 19,700 130 350	9° 19,750 ft 127° 350 kt
18)	DT	18	CRT Corr	38 39 40 34 rest = 2	15,500 0 26 -4	13,360 ft 0° 47° R -5°
19)	СТ	14	CRT	30 31 32 26 rect = 2	2,500 122 ?* 120	4,000 ft/min 122° 19,800 ft 122°
20)	LT	8	CRT Ccr	12 11 9 13 rect = 3	260 20,500 25 280	263° 20,580 ft 33° 275 kt

^{*} Indicates the response "I don't know."

Pilot D

	Maneuver	Flight Segment	Displa	y Question	Reported	Indicated
1)	СТ	16	inst.	31 26 29 28 Correct = 0	?* ?* 300 10	262° 260° 390 kt 16°
2)	C	3	CRT	.5 8 4 6 Correct = 4	355 none 5,800 0	365 kt none 5,800 ft/min 0°
3)	DT	20	inst.	39 34 37 36 Correct = 2	3 -6 19,000 300	0° -5° 20,000 ft 315 kt
4)	СТ	14	inst.	32 25 27 30 Correct = 3	19,000 260 25 4,000	19,800 ft 255 kt 27° 4,000 ft/min
5)	С	1	CRT	3 1 2 7 Correct = 3	0 19,800 20,000 16	0° 19,670 ft 19,830 ft 23°
6)	СТ	13	CRT	27 25 26 31 Correct = 1	40 300 90 90	40° 345 kt 126° 127°
7)	С	4	inst.	7 2 5 4 Correct = 4	12 20,000 360 3,000	12° 19,920 ft 350 kt 3,100 ft/min
8)	D	12	inst.	23 18 21 20 Correct = 2	0 360 15,000 19,000	0° 290 kt 15,170 ft 20,240 ft

^{*} Indicates the response "I don't know."

	Maneuver	Flight Segment	Display	Question	Reported	Indicated
9)	LT	5 .	CRT	11 9 10 15 Correct = 3	20,300 30 19,000 275	20,400 ft 34° 19,810 ft 275 kt
10)	LT	8	inst.	15 10 13 12 Correct = 3	280 20,000 280 270	290 kt 19,690 ft 275 kt 263°
11)	ז ם	18	inst.	40 33 35 38 Correct = 3	45 140 300 13,000	47° 167° 295 kt 13,360 ft
12)	D	10	inst.	24 17 19 22 Correct = 4	0 -12 310 0	0° -7° 300 kt 0°
13)	СТ	15	CRT	29 32 28 30 Correct = 2	350 15,000 8 1,000	345 kt 20,140 ft 11° 4,300 ft/min
14)	С	2	inst.	8 1 3 6 Correct = 4	none 19,500 0 0	none 19,880 ft 0° 0°
15)	DT	17	CRT	35 33 34 39 Correct 3	300 190 -2 0	300 kt 216° -1° 0°
16)	D	9	CRT	19 17 18 23 Correct = 4	310 -2 300 0	315 kt -1° 310 kt 0°

	Maneuver	Flight Segment	<u>Display</u>	Question	Reported	Indicated
17)	DT	19	CRT	37 40 35 38 crect = 3	19,900 26 360 15,000	19,890 ft 32° 350 kt 15,230 ft
18)	LT	7	CRT	13 16 12 14 rrect = 4	275 270 90 275	270 kt 265 kt 92° 270 kt
19)	LT	6	inst.	16 9 11 14 rrect = 1	260 25 20,500 260	235 kt 32° 20,950 ft 245 kt
20)	D	11	CRT	21 24 20 22 rrect = 3	17,000 2 20,100 U	15,490 ft 2° 20,130 ft 0°

APPENDIX K: TEST IP BRIEFING

You are being asked to participate in a test which is being developed for future evaluation of cockpit displays. In the present instance, we are limiting the display to the flight performance indications, specifically a) airspeed, b) airplane pitch and bank attitude, c) altitude, d) vertical velocity, and e) heading.

You will see two types of displays, standard instruments and digital presentation on a cathode ray tube. These have not been chosen because of a question about their relative effectiveness but because of their dissimilarity. It's rather like the difference between a traditional watch with dial and hands and the new digital watches; one format may be good in one situation while the other may best suit another.

It is important that you know that, although we ask you to work sincerely at the task, we are not testing your ability but rather the efficiency of our approach to the evaluation of displays. Since you will see both types of displays, we can compare your performance with one type against your performance with the other type. Thus we are not concerned with comparitions between your performance and someone else's, only with how effective is our approach to display evaluation.

In this, the initial stage of research in this area - information displays at an instructor/operator station in conjunction with flight simulator training - some artificialities are required. For example, we will ask you to view a series of short one or two minute flight segments without describing the maneuver before its presentation. The information presented to you will be limited to that mentioned earlier; airspeed, attitude, altitude, vertical velocity, and heading. This will be shown either in digital ferm on a cathode ray tube or on standard instruments, circular dial with pointer except for the attitude indicator. The arrangement will be standard with the airspeed on the left, attitude indicator in the middle above the heading indicator, and altitude on the right next to the VVI. The digital format on the cathode ray tube (located above the standard instruments, which will be covered during the cathode ray tube presentations) will be arranged in the same manner as the standard instruments.

After each flight segment presentation, you will be asked questions about the information shown in the display. These questions will be concerned with the values displayed at various points in the maneuver such as maximum and minimum altitude, attitude, airspeed, vertical velocity, or heading at various points in the maneuver. You are being asked to remain alert to all of the five instrument indications throughout the short flight segment, this being the reason for your not being told about the maneuver beforehand.

The questions have been selected to represent typical student errors in flying in a simulator and will therefore be relevant to the maneuver presented. However, since you will not be told about the maneuver prior to the presentation, the questions will be related to identifiable portions of it such as beginning airspeed in a turn or altitude at level-off in a climb.

This research is being conducted as part of an Air Force contract with the Boeing Company. As a research and development effort conducted under contract, the Air Force is, of course, not responsible for the specifics of this test. However, the Company has obvious interest in its success. We, therefore, ask you to do your best in the task in which you are participating, and we welcome any suggestions you may have for improving the quality of this evaluation technique.

APPENDIX L: DATA SUMMARY BY MANEUVER AND INDICATION

				NSTRE	INSTRUMENTS					CRT	11		
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TOTAL CORREC	POSS. CORRECT CORRECT	36 28 78	36 25 69	\$ 50	44 25 57	20 18 90	ည် စ လိ	36 18 50	36 25 72	∞ w ∞	44 30 68	20 12 60	16 13 81
				8%	OVERALL					64 % OV	OVERALL		

A - ALTITUDE H - READING VV - VERTICAL VELOCITY 68% OVERALL:

AS - AIR SPEED R - ROLL P - PITCH

APPENDIX M: LEARNING EFFECTS

Number of Correct Answers

Flight Segment Order	P.	L:	Pilot C	Б
1 ? 4 5	1	0 1 0 1 9	4 4 2 3 17	0 2 3 3 12
6 7 9 9 10	3 4 3 4 18	2 1 0 2 4	0 2 2 2 3 12	1 4 2 3 3 13
11 12 13 14 15	2 3 3 2 4	2 0 3 3 3	3 3 3 4	3 2 4 3
16 17 10 19 00	2 2 3 , 1	1 3 (1 11	3 4 2 5 3 14	2 3 4 1 3 1